

$$\begin{aligned} \lceil \leq \rceil \leq \lceil \approx \rceil \cap \mathbb{L} \text{---} \mathbb{L} \text{F} \lceil + \approx \rceil \text{---} \leq \lceil \approx \rceil \int \rceil \approx \rceil \text{---} \\ \lceil \lceil \approx \rceil \leq \sqrt{\text{r}} \text{ } \text{ } \rceil \text{---} \text{---} \text{---} \infty \sqrt{\text{---}} \text{---} \mathbb{L} \sqrt{\rceil} \leq \text{ } \text{ } \\ \approx \lceil \lceil \infty \leq \Delta \leq \rceil \approx \infty \Delta \leq \lceil \mathbb{L} \sqrt{\rceil} \end{aligned}$$

$$\begin{aligned} \mathbb{L} \sqrt{\lceil + \Delta \approx \rceil} \mathbb{L} \Delta \leq \geq \text{---} \text{---} \int \sqrt{\cap \mathbb{L} \approx \rceil} \rceil \text{F} \geq \\ \approx \lceil \rceil \leq \text{---} \approx \lceil \Delta \leq \geq \rceil \rceil \leq \approx \cap \leq \approx \mathbb{L} \\ \leq \lceil \approx \rceil \leq \leq \lceil \text{---} \sqrt{\lceil} \sqrt{\Delta} \sqrt{\text{---}} \text{---} \lceil \text{---} \mathbb{L} \sqrt{\text{---}} \end{aligned}$$

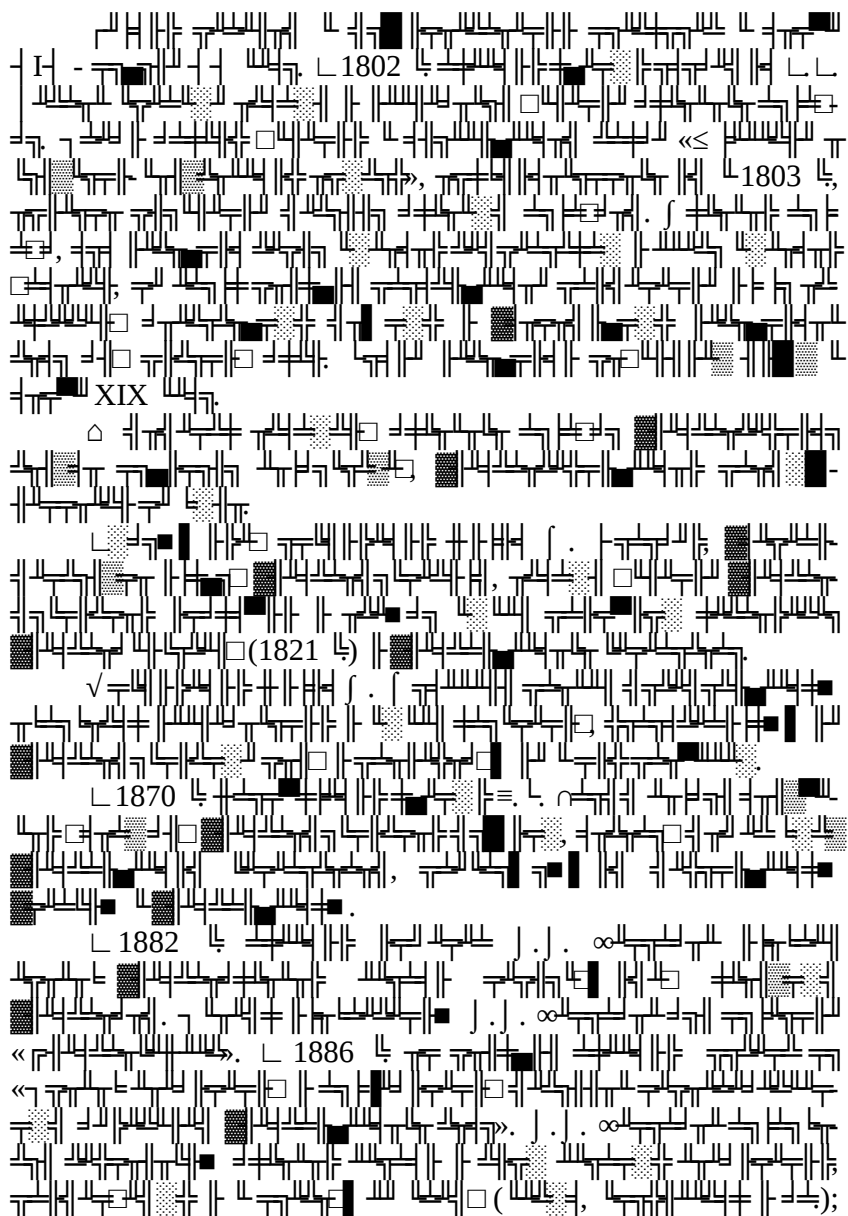
$$\lceil . \lceil . \rceil \text{---} \text{---} \blacksquare \text{---} \text{---}$$

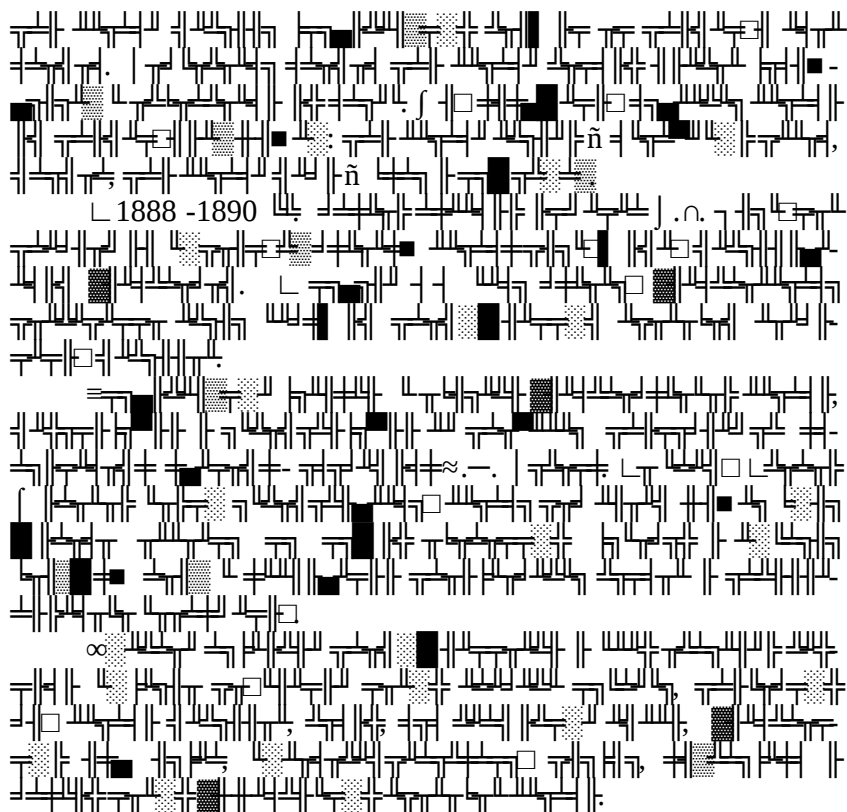
$$\begin{aligned} \text{---} \lceil \rceil \text{---} \mathbb{L} \rceil \text{F} \approx \lceil \approx \mathbb{L} \int \text{F} \lceil \mathbb{L} \sqrt{\text{---}} \text{ } \Delta \leq \leq \\ \approx \lceil \text{---} \rceil \mathbb{L} \sqrt{\text{---}} \mathbb{L} \lceil \sqrt{\lceil + \leq \rceil} \text{---} \lceil \mathbb{L} \text{---} \approx \rceil \leq \leq \end{aligned}$$

$$\Delta \text{---} \lceil \lceil \lceil \approx \Delta \mathbb{L} \text{---} \approx \Delta \text{---} \leq \geq$$

$$\mathbb{L} \sqrt{\lceil + \Delta \approx \rceil} \mathbb{L} \textbf{2017}$$

© 
2017

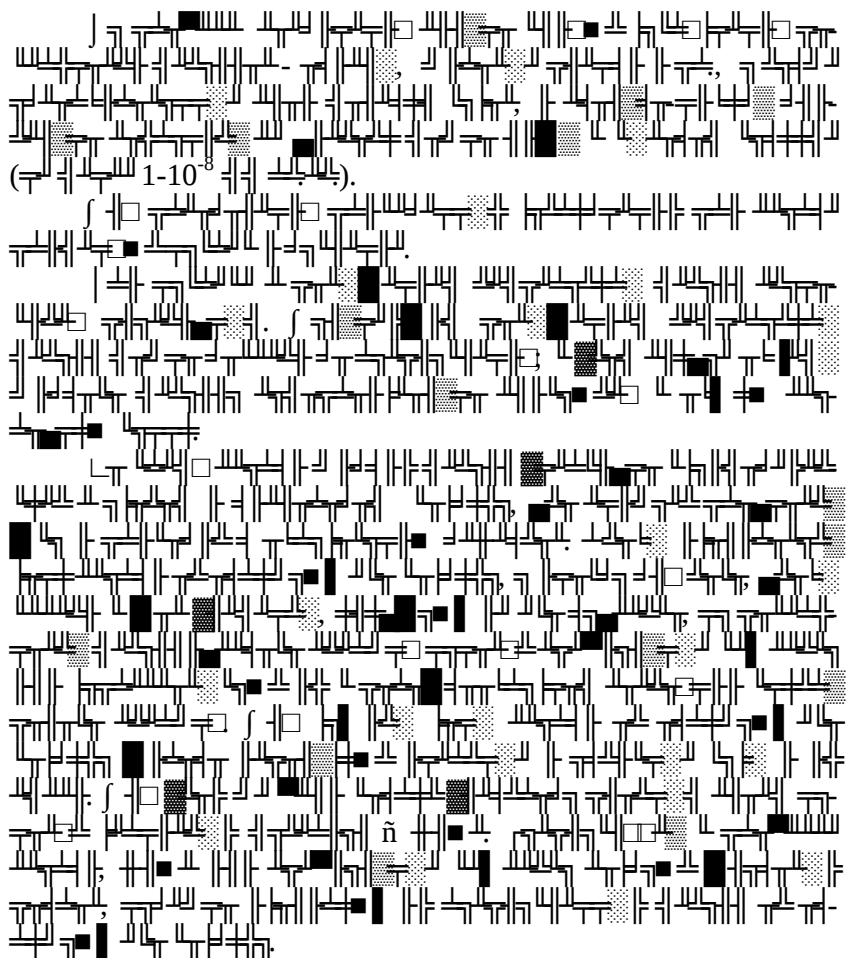




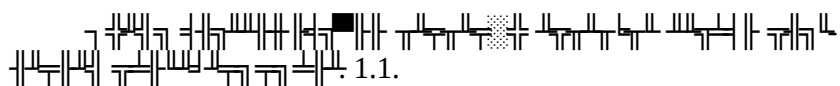
1.

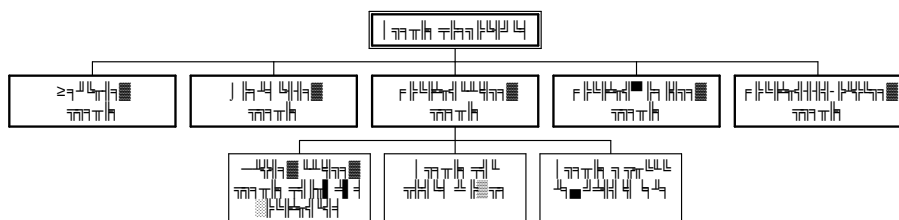
1.1.
 1.2.
 1.3.

1.1.



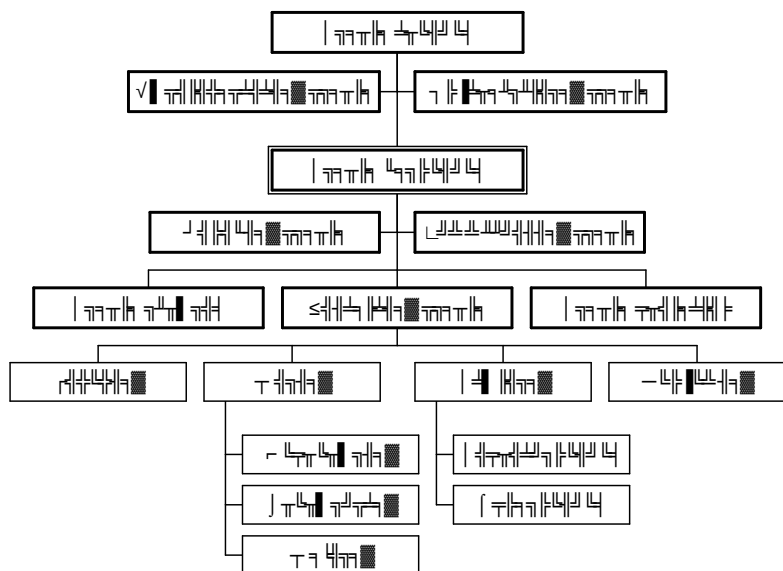
1.2. $\triangle$





1.1. Δ אנשים חסידים 80-90 א.

1.2. אנשים חסידים 80-90 ב.

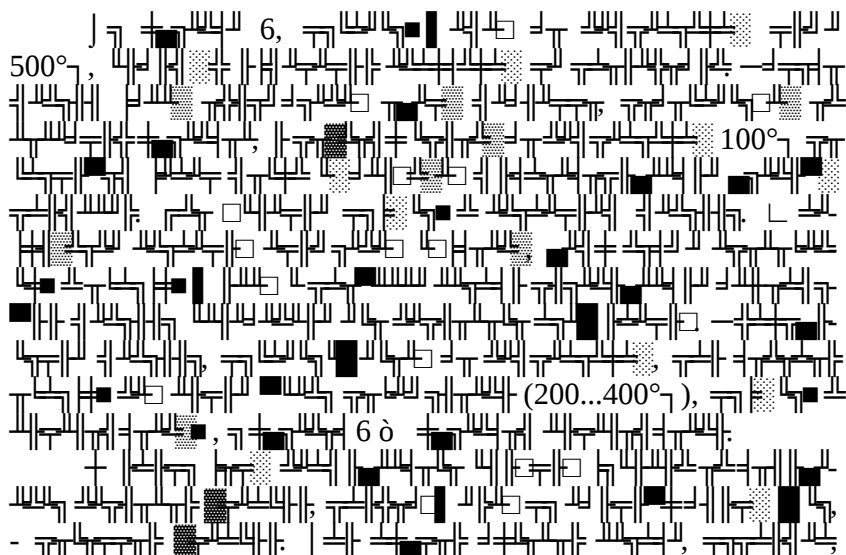
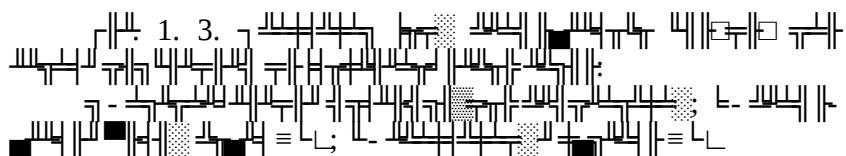
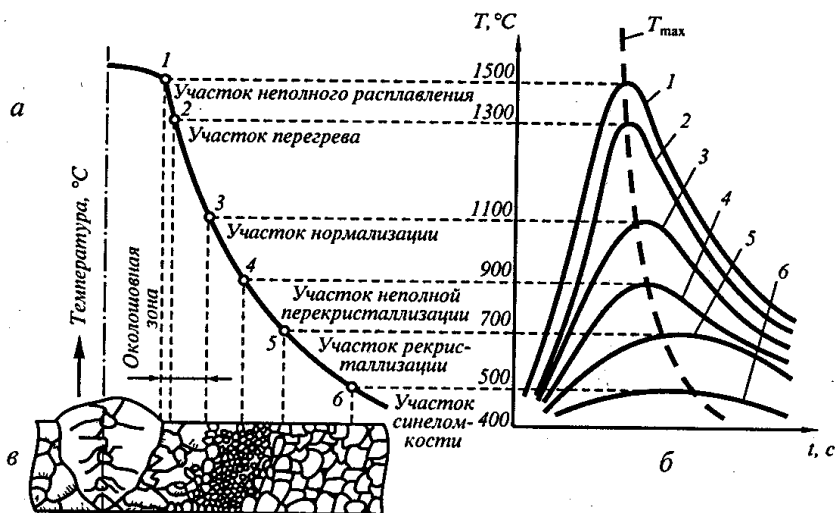


1.2. Δ אנשים חסידים 70-80 א.

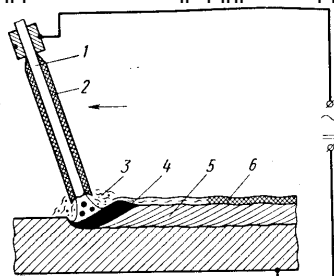
1.3. אנשים חסידים 70-80 ב.

אנשים חסידים 70-80 ג.

2. 1130° ,
 $900 \dots 1100^{\circ}$
 4 $723 \dots 900^{\circ}$.
 3,
 5 $500 \dots 723^{\circ}$.



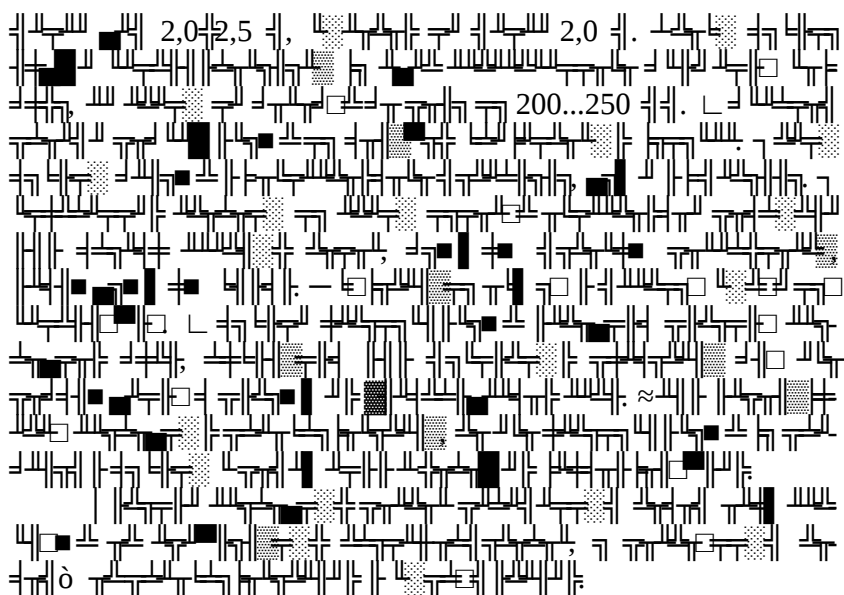
0,5 ñ 1,1 ñ 3 ñ 6 ñ 90-350 √ 18-30 √



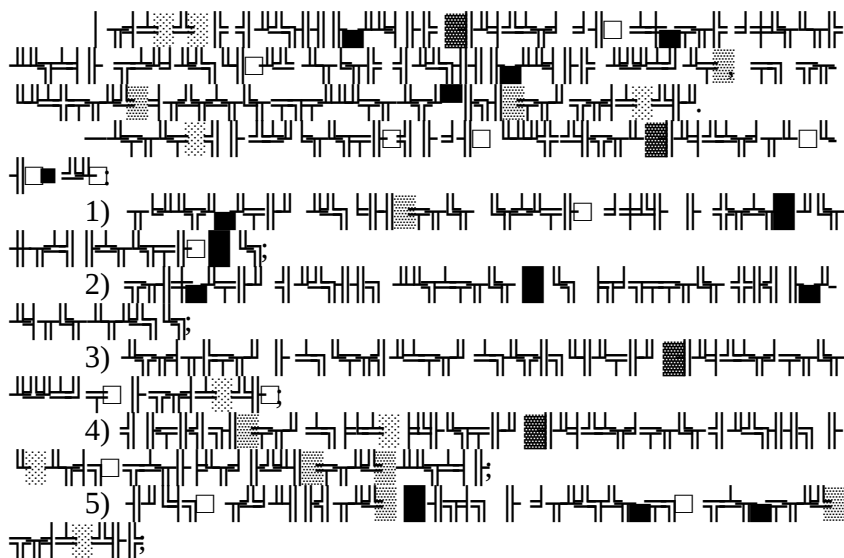
2.1. 1 ñ 2 ñ 3 ñ 4 ñ 5 ñ 6 ñ

2.2. -

~



2.3.





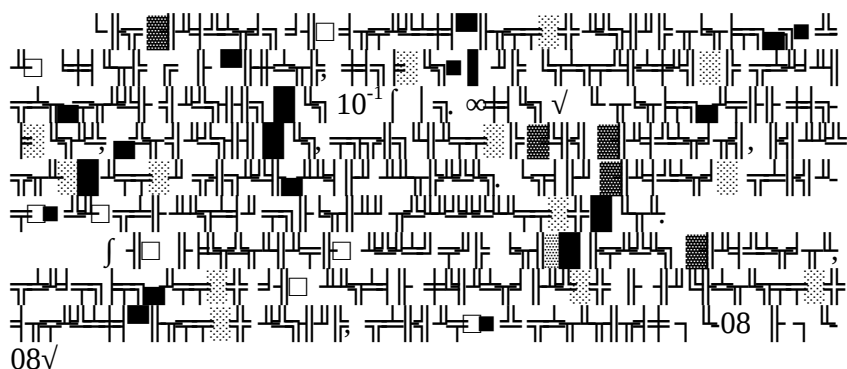
$$\text{Na}_2\text{O} \cdot \text{SiO}_2 \cdot \text{---} \text{---} m = \frac{\text{SiO}_2}{\text{Na}_2\text{O}} \text{---} \text{---}$$

Figure 4 shows a musical score for a string quartet. It consists of four staves, each with a different instrument part. The notation includes various musical symbols such as notes, rests, and dynamic markings. The score is written in a standard musical notation style, with a key signature of one flat and a 4/4 time signature. The first staff is for the Violin I, the second for Violin II, the third for Viola, and the fourth for Cello. The score includes a variety of musical notations, including eighth notes, quarter notes, and half notes, as well as rests and dynamic markings like *mf* and *f*. The score is divided into measures by vertical bar lines, and there are repeat signs and first/second endings indicated. The overall structure of the score is complex, with many measures and a variety of musical notations.

0,035% (0,5 = 1,5% n 0,3
0,6% Si).

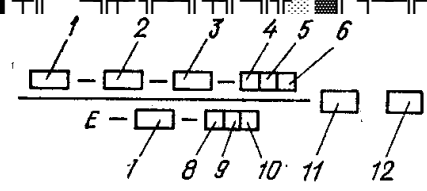
($\sqrt{1-3}$, $\sqrt{1-4}$, $\sqrt{1-3}$, $\sqrt{1-4}$)

2.



08√
 (2.2):

- 1 -
- 2 -
- 3 -
- 4 -
- 5 -
- 6 -
- 7 -
- 8 -
- 9 -
- 10 -
- 11 -
- 12 -

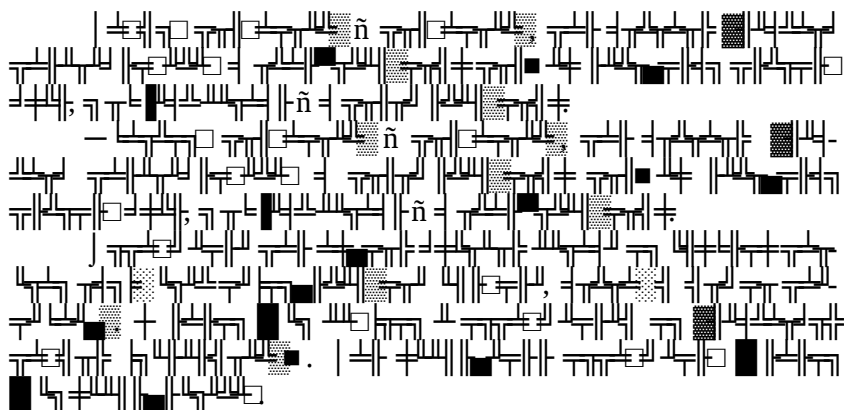


2.2.

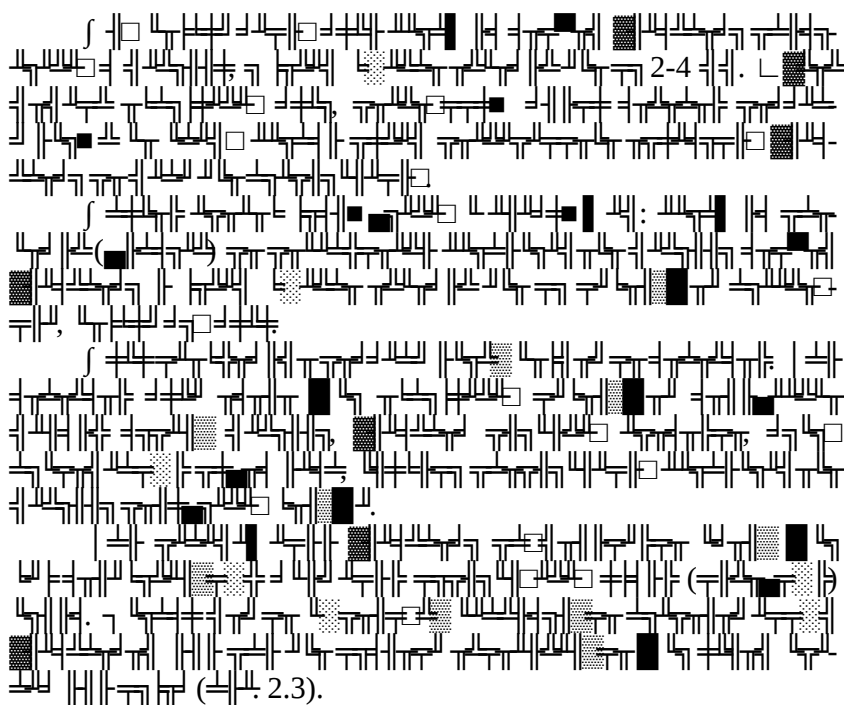
$4\delta \ 5$, U -
 $(\dots)$
 5 .
 5 .
 Δ . Δ .

$$I_{III}=(20+6d)d,$$

$I_c \ll \delta$, A ;
 $d \delta$.
 $1,5 \ d$.
 $10\delta \ 15\%$, $3 \ d\delta$, $10\delta \ 15\%$
 $10\delta \ 15\%$, $15\delta \ 20\%$
 δ .
 $\dots$



2.5.



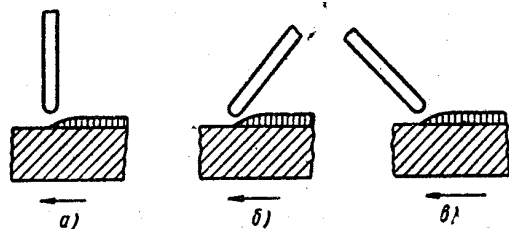
2-4. 

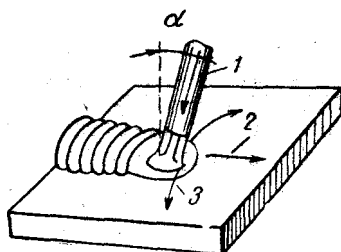
()

()

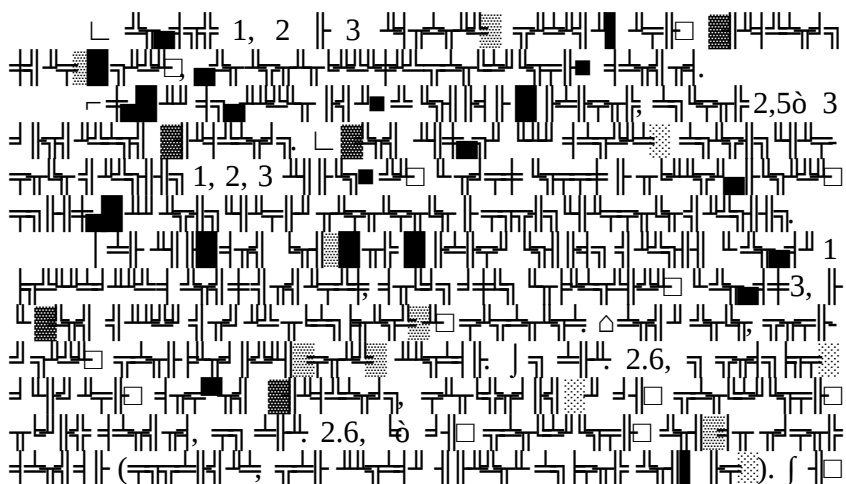
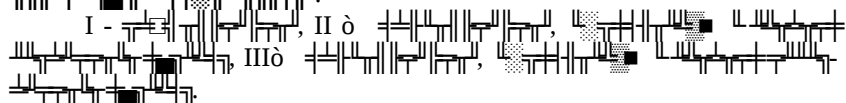
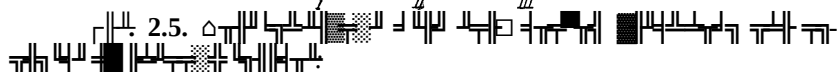
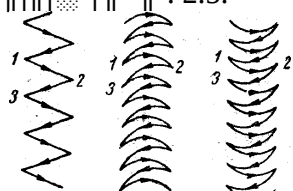
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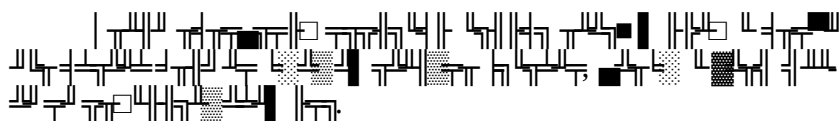
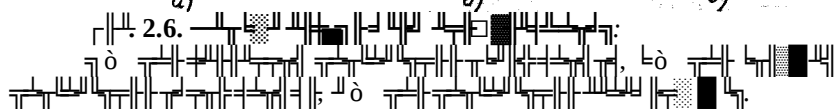
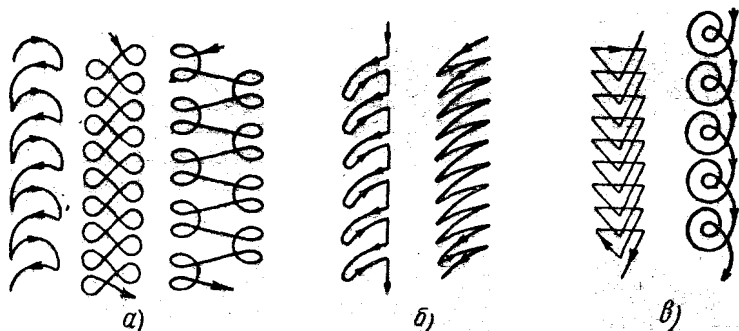
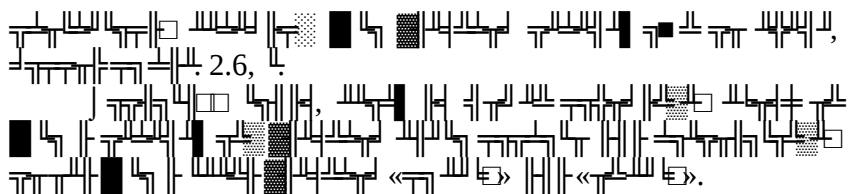
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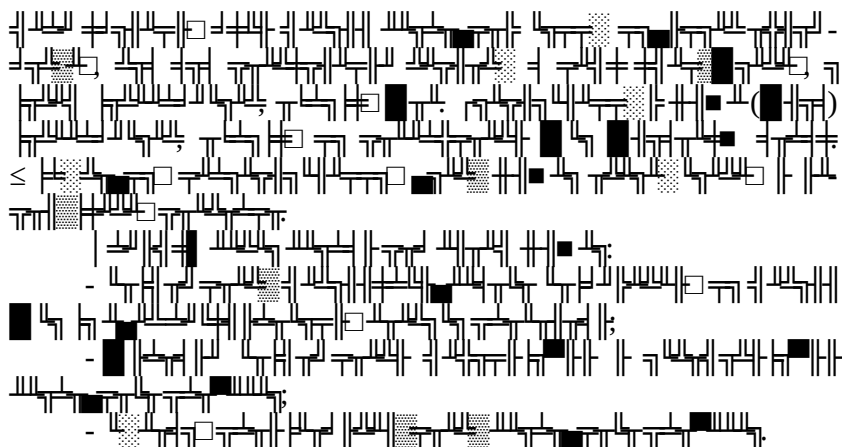




2.4. |







3.1. 1 ñ 2 ñ 3 ñ 4 - 5 ñ 6 ñ 7 ñ 8 ñ 9 ñ

3.2. ,

L 22460 70 « 0,3; 0,5; 0,8; 1; 1,2; 1,4; 1,6; 2; 2,5; 3,0; 4; 5; 6; 8; 10 12 .

$2 \tilde{n} 6$.
 $1,6 \tilde{n} 12,0$
 $1,5\delta 40$

77

$0,12\%$
 $08, \gamma 08\sqrt{\gamma}, \gamma 08\sqrt{\gamma}, \gamma 08\sqrt{\gamma}, \gamma 10\sqrt{\gamma}, \gamma 10\sqrt{\gamma};$
 $08\sqrt{\gamma}, \gamma 08\sqrt{\gamma}, \gamma 12\sqrt{\gamma}, \gamma 12\sqrt{\gamma};$
 30

$12-11, \gamma 12-13, \gamma 08-14$

1%
 $3.1.$

$3 \gamma 10\sqrt{\gamma}, \gamma 2246-70 \tilde{n}$
 $3 \gamma 0,10\% 2\%$

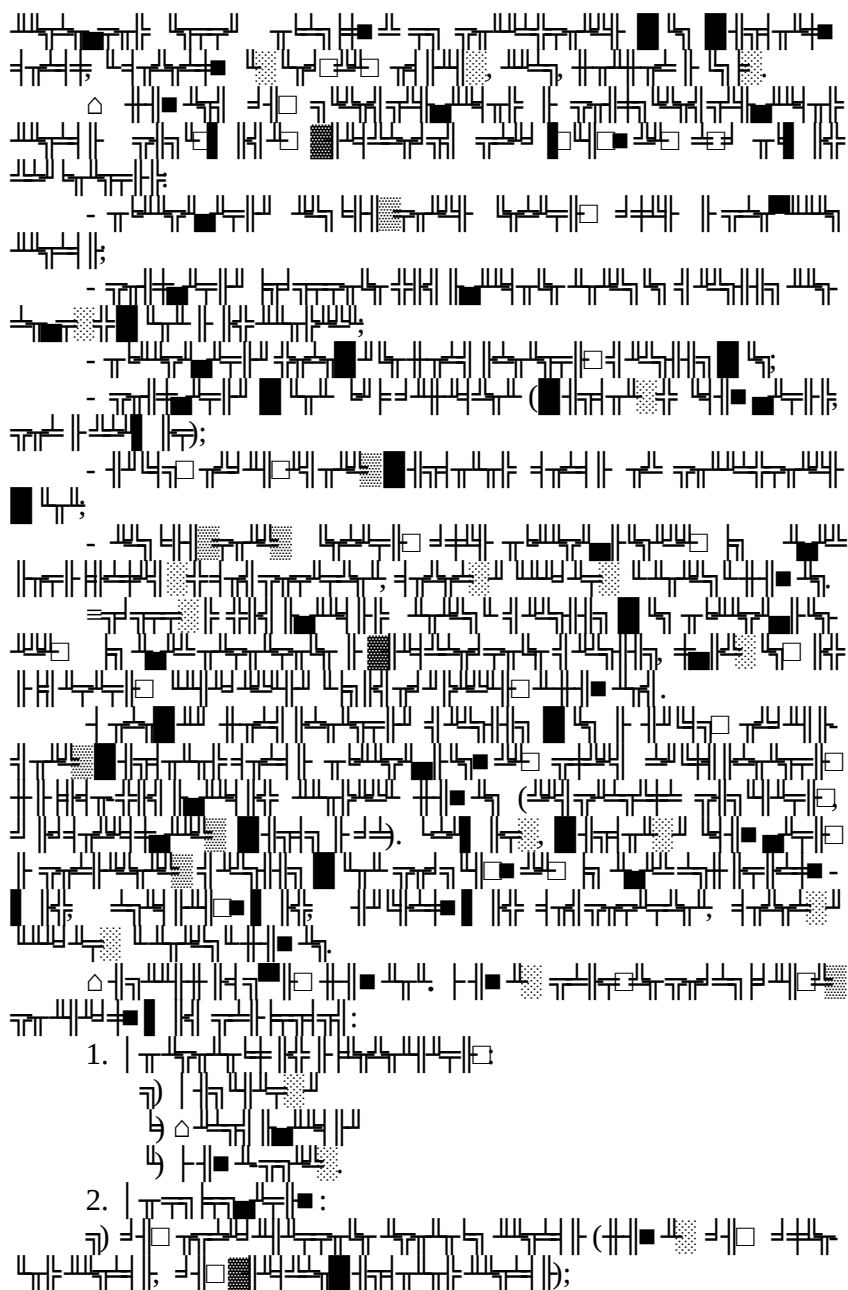
1% .

3.1

$\sqrt{\quad}$	N	$\sqrt{*}$
	Nb	∞
	W	L
	Mn	$\cap$
	Cu	$\int$
	Se	$\approx$
	Co	$\triangle$
	Mo	$\int$
	Ni	
∞	B	Γ
$\triangle$	Si	$\int$
	Ti	L
	V	$\vdash$
	Cr	$\vdash$
$\sqrt{\quad}$	Al	$\int$

* .

0,25-4 .

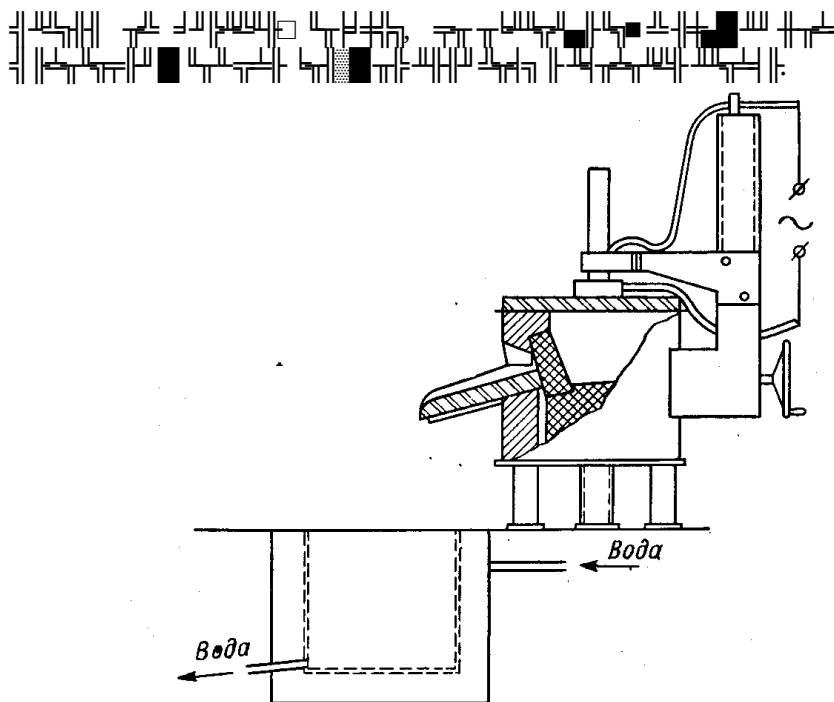


3.2

3.2

	%, %								
	SiO ₂	MnO	CaO	MgO	Al ₂ O ₃	CaF ₂	Fe ₂ O ₃	S	P
√ -348-√	41,0- 44,0	34,0- 38,0	≤ 6,5	5,0- 7,5	≤ 4,5	4,0- 5,5	2,0	0,15	0,12
┐┐-45	38,0- 44,0	38,0- 44,0	≤ 6,5	≤ 2,5	≤ 5,0	6,0- 9,0	2,0	0,15	0,15
√ -348- √	41,0- 44,0	34,0- 38,0	≤ 6,5	≤ 4,5	≤ 4,5	3,5- 4,5	2,0	0,15	0,12
┐┐-45┐	38,0- 44,0	38,0- 44,0	≤ 6,5	≤ 2,5	≤ 5,0	6,0- 9,0	2,0	0,15	0,10
√ -60	42,5- 46,5	36,0- 41,0	3,0- 11,0	0,5- 3,0	≤ 5,0	5,0- 8,0	1,5	0,15	0,15
┐┐-9	38,0- 41,0	38,0- 41,0	≤ 6,5	≤ 2,5	10,0- 13,0	2,0- 3,0	2,0	0,10	0,10
√ -8	33,0- 36,0	21,0- 26,0	1,0- 7,0	5,0- 7,5	11,0- 15,0	13,0- 19,0	1,5-3,5	0,15	0,15
√ -20┐, √ -20┐┐, √ -20┐	19,0- 24,0	≤ 0,5	3,0- 9,0	9,0- 13,0	27,0- 32,0	25,0- 33,0	1,0	0,08	0,05
√ -22	18,0- 21,5	7,0- 9,0	12,0- 15,0	11,5- 15,0	19,0- 23,0	20,0- 24,0	1,0	0,05	0,05
√ -26┐, √ -26┐┐, √ -26┐	29,0- 33,0	2,5- 4,0	4,0- 8,0	15,0- 18,0	19,0- 23,0	20,0- 24,0	1,5	0,10	0,10

√ | -26┐, √ | -26┐┐, √ | -26┐
17┐, √ | -43┐, √ | -47┐



3.2.

3.3

3.3

√ -348- √			0,35-3,0	1,3-1,8
√ -348- √			0,25-1,60	
┐┐-45			0,35-3,00	
┐┐- 45			1,25-1,60	
┐┐-9			0,25-1,60	
√ -60			0,35-4,00	0,7-1,0
√ -20			0,35-4,00	
√ -26			0,35-3,00	
√ -8			0,25-2,50	1,5-1,8
√ -20┐			0,35-3,00	1,2-1,7
√ - 20┐			0,25-1,60	
√ -22			0,25-2,50	1,5-1,8
√ -26┐			0,25-2,50	1,3-1,8

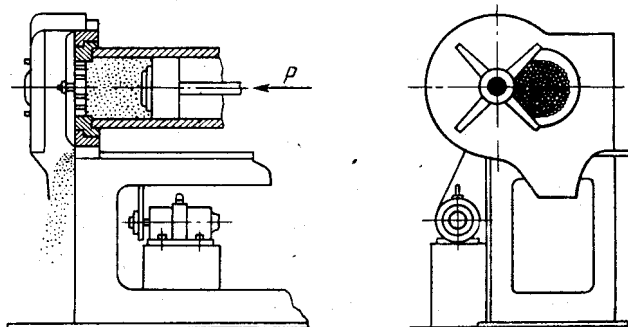
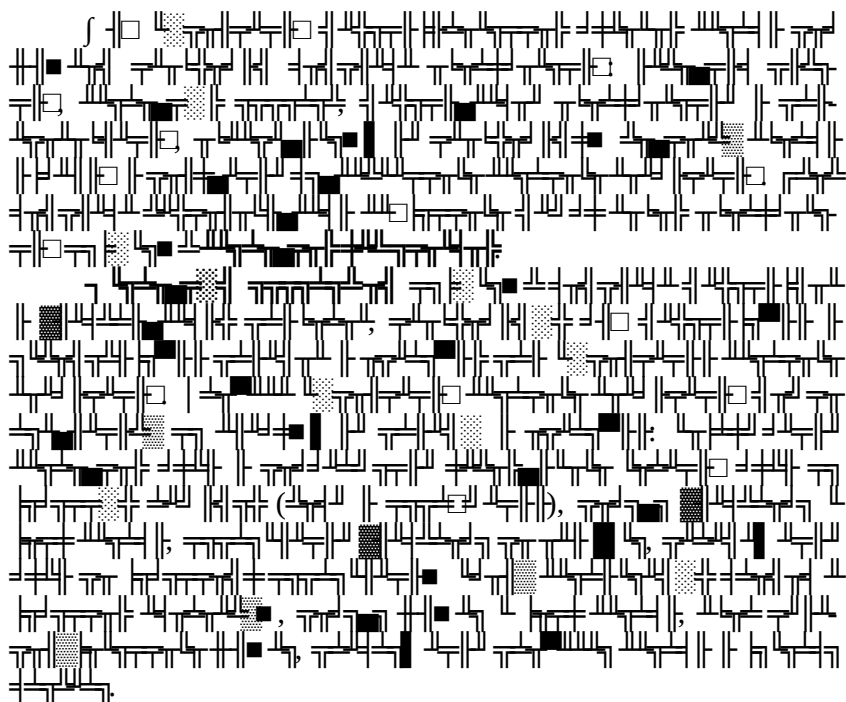
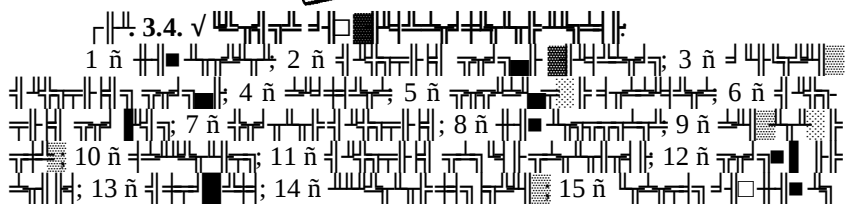
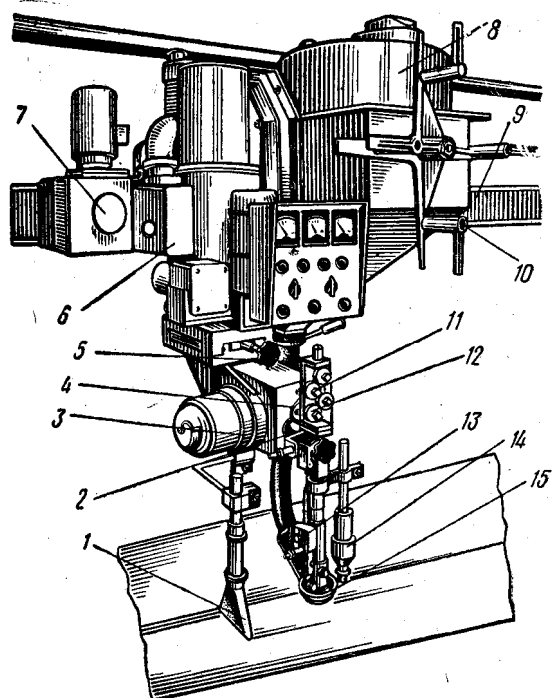
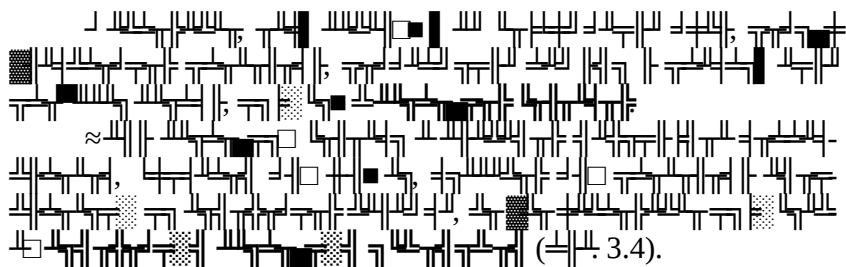
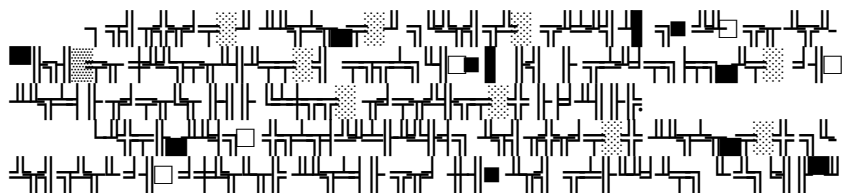


Fig. 3.3. —

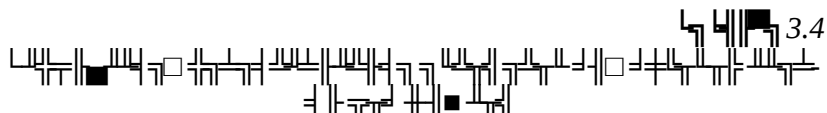
3.3. —







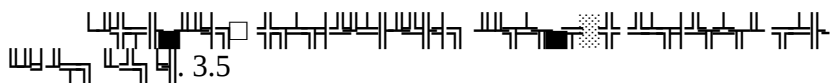
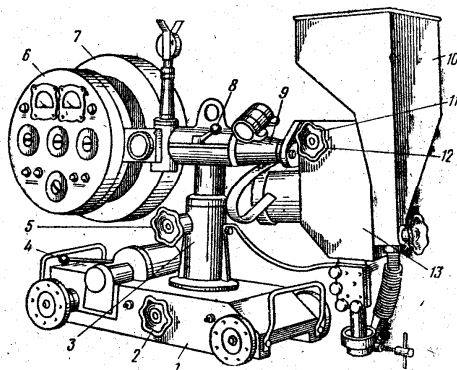
3.4.



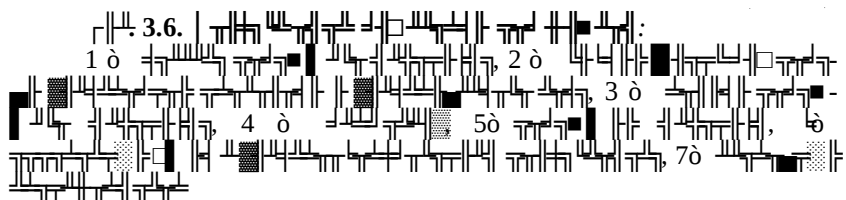
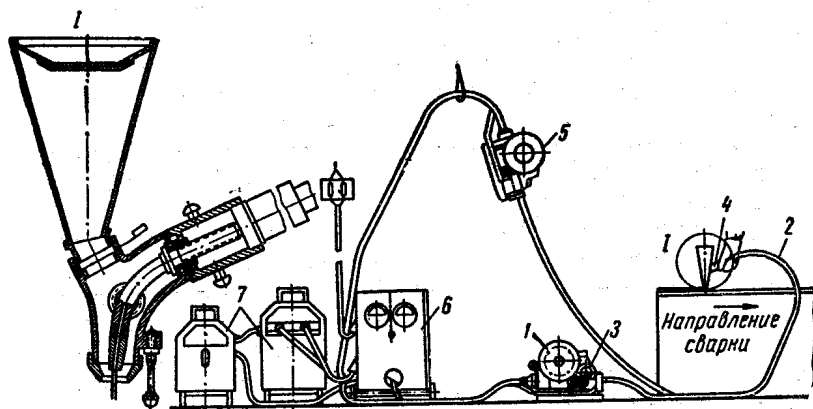
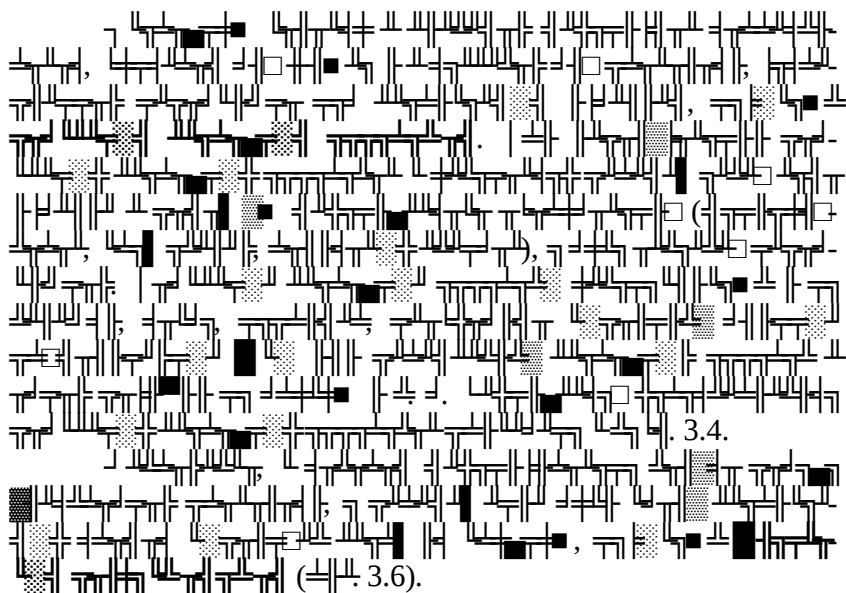
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$\sqrt{-1416}$	1000	2-5	1,4-13,9	0,3-3,3	
$\sqrt{-1425}$	1000	4-5	1,4-13,9	0,3-3,3	
$\sqrt{\infty} \triangle$	1000	3-6	1,2-3,9	0,6-2	
$\sqrt{-1423}$	315	1,6-3	1,3-12,5	-	
$\cap \vdash$ 1001	1000	3-5	1,5-14,8	-	

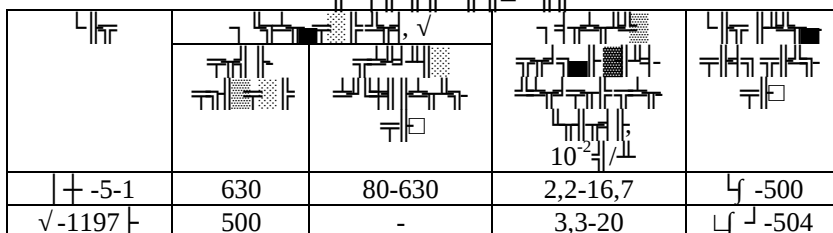


(3.5).



$\sqrt{f}$ -501	500	1,6-2	0,8-2,0	0,4-1,9	$\sqrt{f}$ -504
$\sqrt{f}$ -17 -1	1000	1,6-5	1,4-11,1	0,4-3,5	$\sqrt{f}$ -1001
$\sqrt{f}$ -1000-4	1000	2-5	1,7-10	0,3-3,3	$\sqrt{f}$ -1001
$\sqrt{f}$ -1000-5	1000	2-5	1,7-10	0,3-3,3	$\sqrt{f}$ -1001
$\sqrt{f}$ -1001	1000	2-5	0,4-10	0,3-3,3	$\sqrt{f}$ -1001
$\sqrt{f}$ -1004	1000	2-5	0,5-10	0,3-3,3	$\sqrt{f}$ -1001
$\sqrt{f}$ -1602	1600	3-6	0,5-10	0,3-3,3	$\sqrt{f}$ -1601





1. $I_c \approx (80 - 100)h_1$,
 $h_1 \approx 0,6 - 0,7s$ ($s \approx 90^\circ$).

$$d_{\text{F}} = 1,13 \sqrt{I_{\text{c}} / j},$$

 jò  √/||².

 (3.7).

 3.7

d_{F}	2	3	4	5	6
$j, \sqrt{ }^2$	65-200	45-90	35-60	30-50	25-45

 3.  √/||²

 (3.7):

 3.7

d_{F}	2	3	4	5	6
$\sqrt{\cdot} \cdot 10^{-3}, \sqrt{\cdot} / \blacksquare$	8-12	12-16	16-20	20-25	25-30

4.  4.

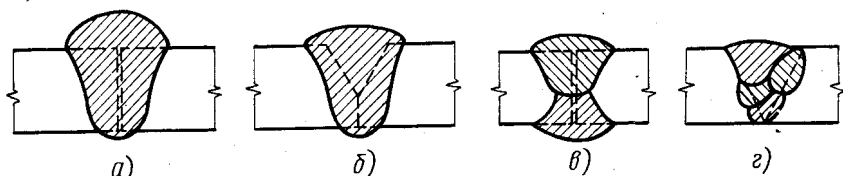
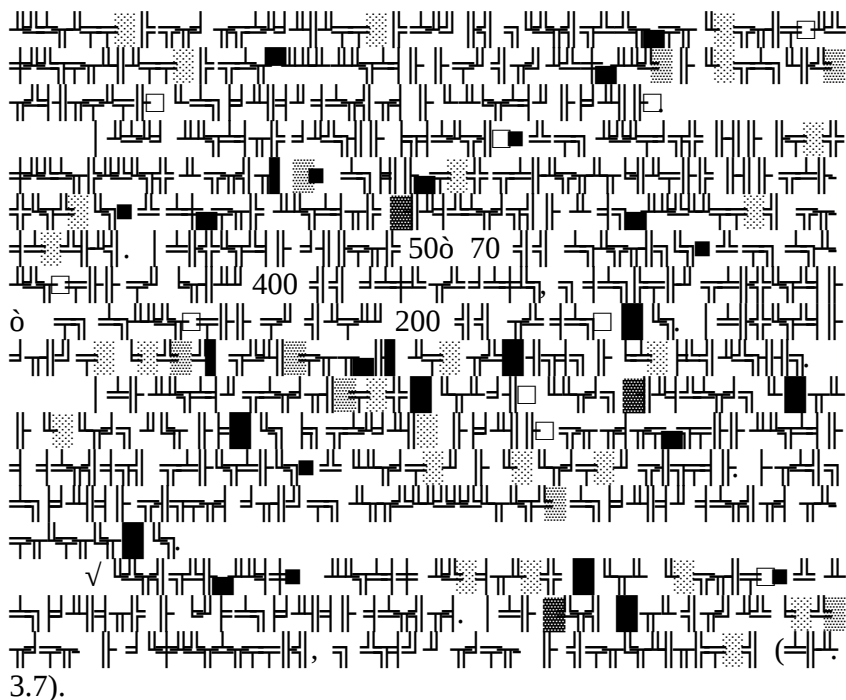
$$U_f = 20 + \frac{50 \cdot 10^{-3}}{\sqrt{d_{\text{F}}}} \pm 1, \text{ L}$$

3.5.  3.5.

 1/3

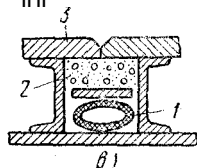
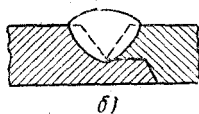
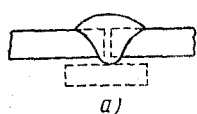
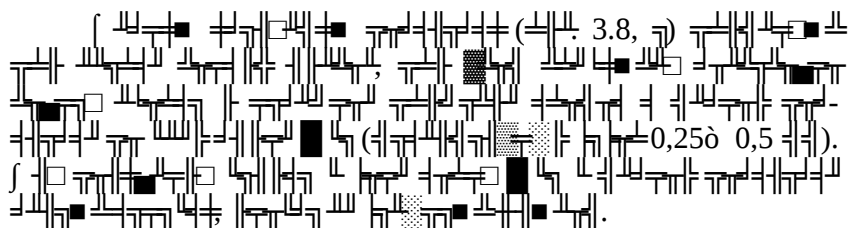
 2/3

 1:1.

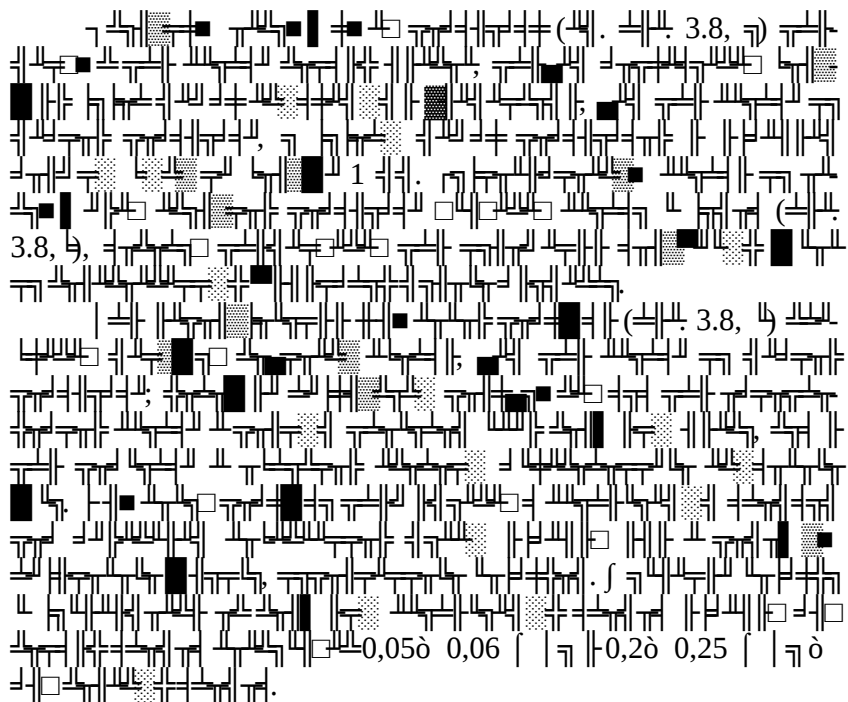


3.7. (), (), (); ()





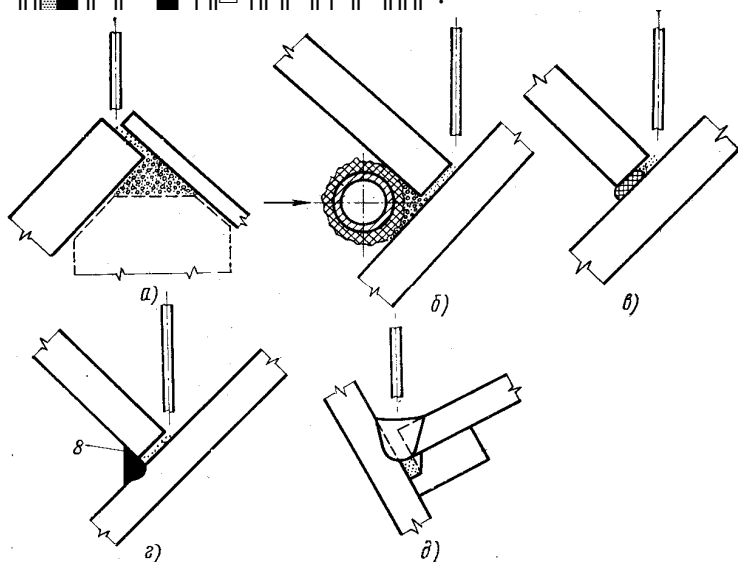
3.8. 



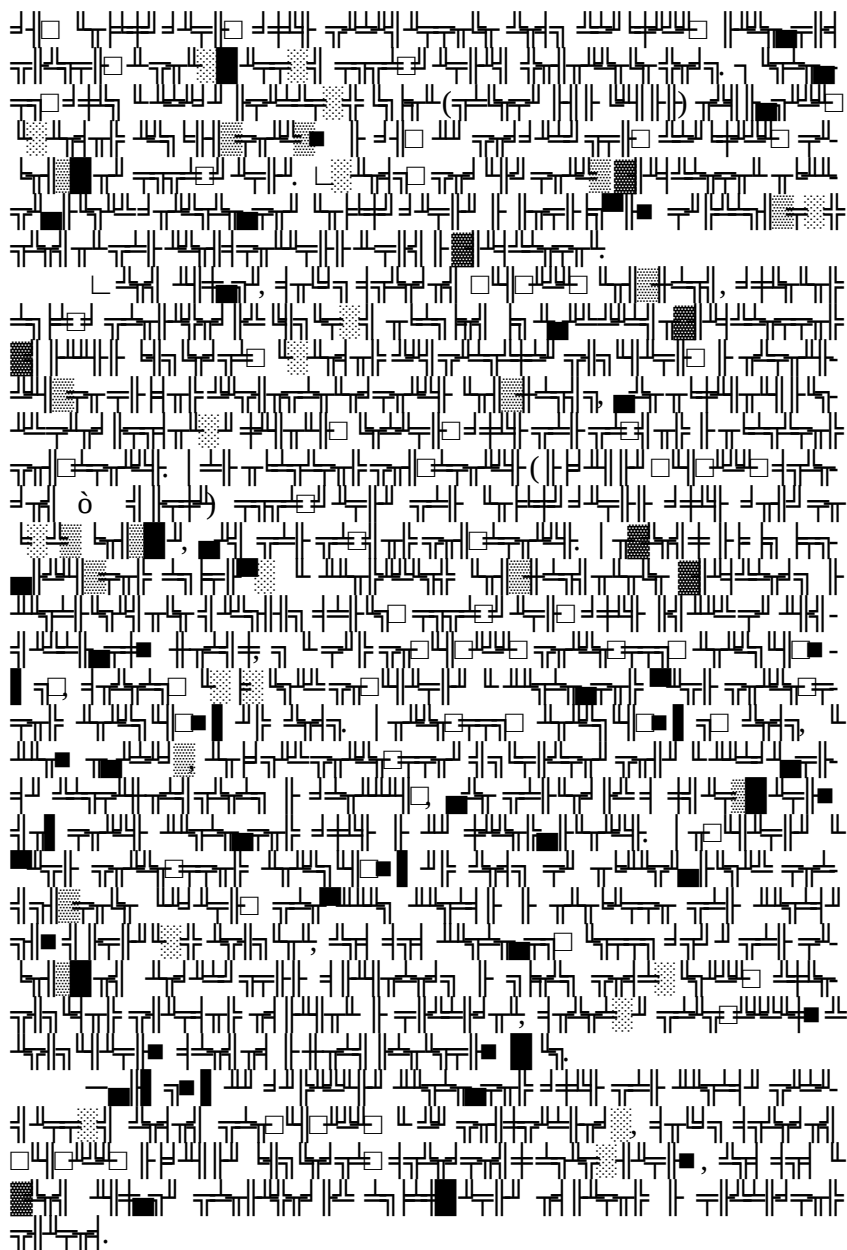
60 ÷ 70% 1 «

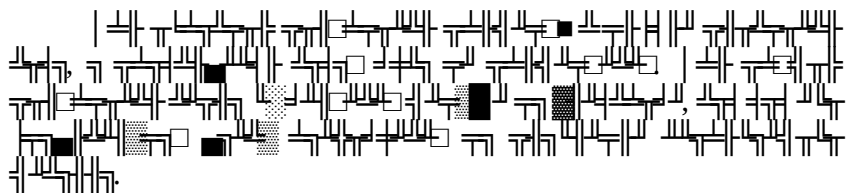
(3.9, 1). 3.9, 2) «

3.9, 3). 3.9, 4) «

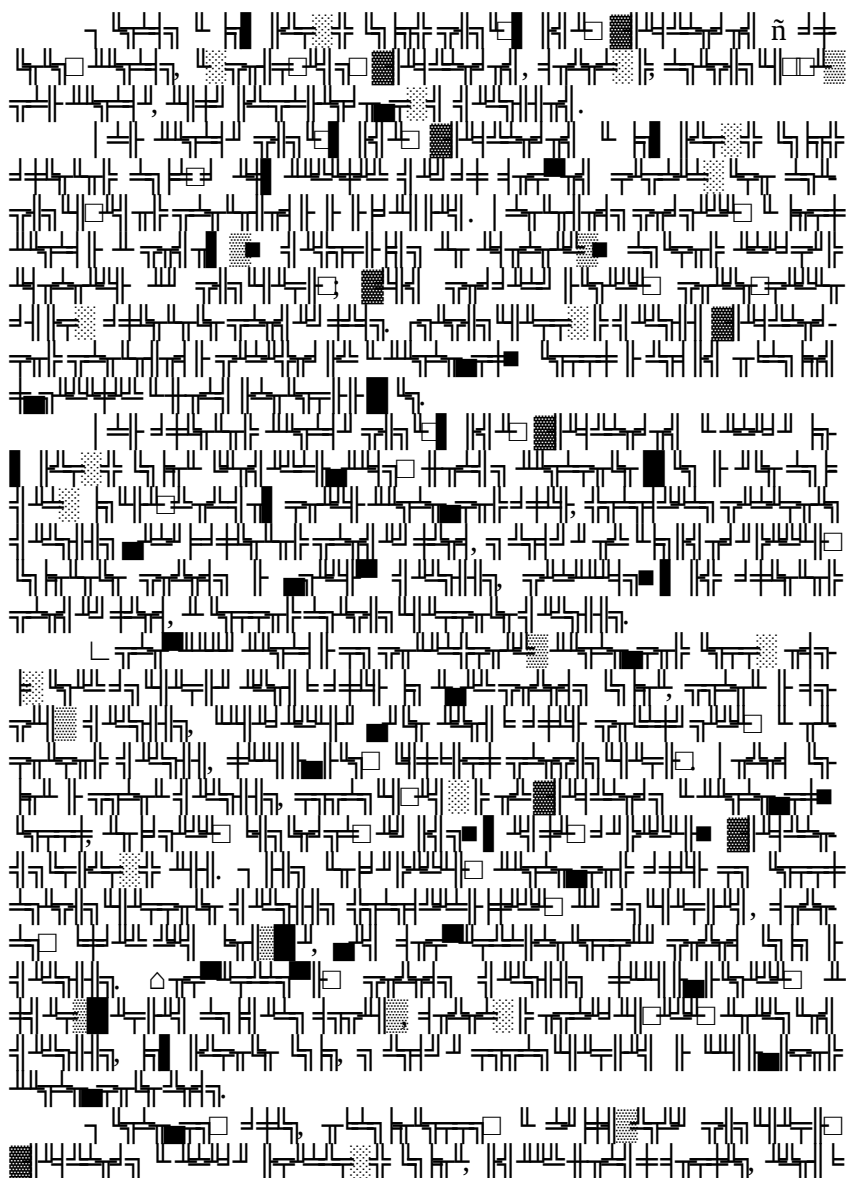


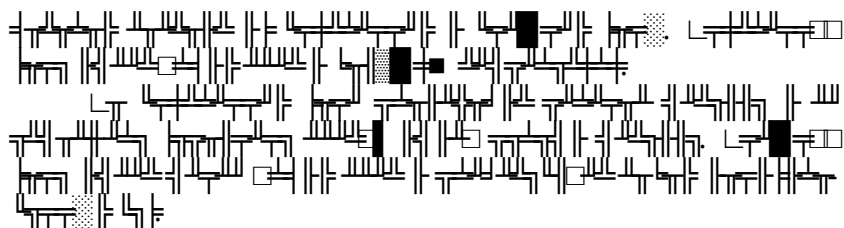
3.9. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100



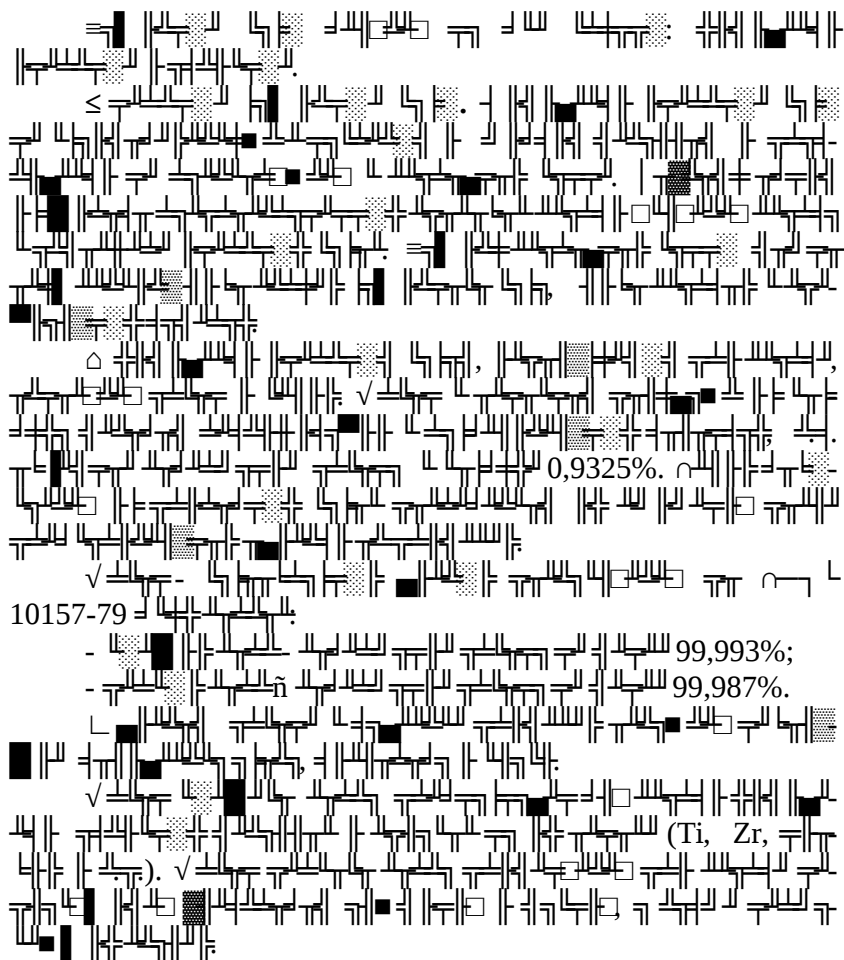


4.3. γ 





4.4.



51-689-79 =

99,995 %;

99,985%.

CO₂, CO, CH₄

40

15

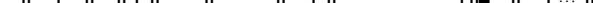
"γ-2".

08~2γ,

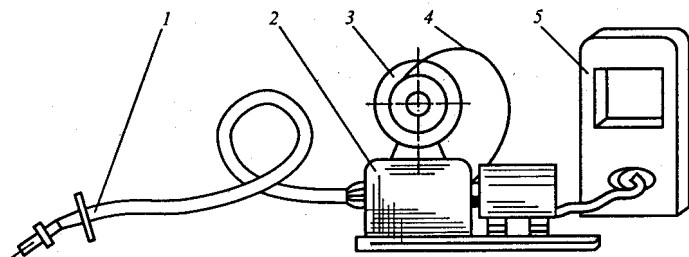
≤

(2 - 5%).

1,5

4.5. — 

$\mathcal{H}_1$ and $\mathcal{H}_2$ are the Hilbert spaces of the two subsystems. The total Hilbert space is $\mathcal{H} = \mathcal{H}_1 \otimes \mathcal{H}_2$. The system is initially in a state ρ_0 on $\mathcal{H}$. The system evolves under a unitary U for a time t . The final state is $\rho_t = U \rho_0 U^\dagger$. The system is then measured on the second subsystem. The measurement outcome is i . The probability of outcome i is $p_i = \text{Tr}(\rho_t (I \otimes E_i))$, where E_i is the measurement operator on the second subsystem. The post-measurement state on the first subsystem is $\rho_i = \frac{1}{p_i} \text{Tr}_2(\rho_t (I \otimes E_i))$. The conditional entropy $H(\mathcal{H}_1 | \mathcal{H}_2)$ is defined as the average entropy of the post-measurement states ρ_i over all outcomes i .



4.1.

1 ñ ; 2 ñ ; 3 ñ ; 4 ñ ; 5 ñ

:
 1. L. ;
 2. ;
 3. ;
 4.

5.

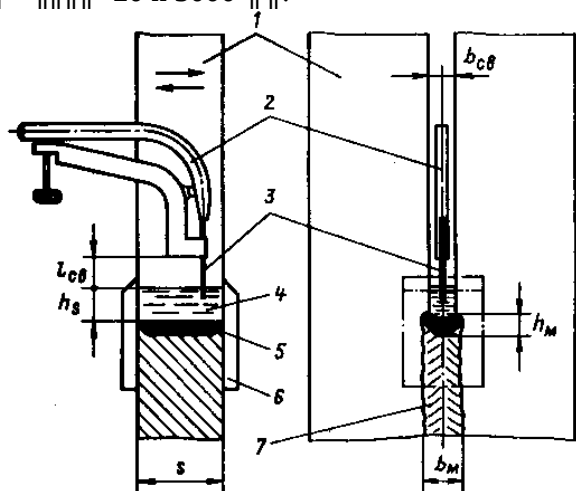
:
 5.1. ;
 5.2. ;
 5.3. ;
 5.4.

;

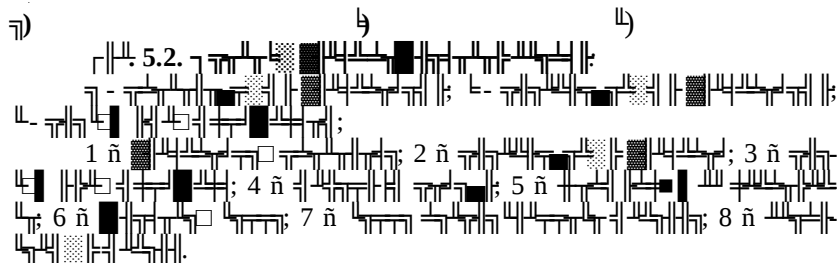
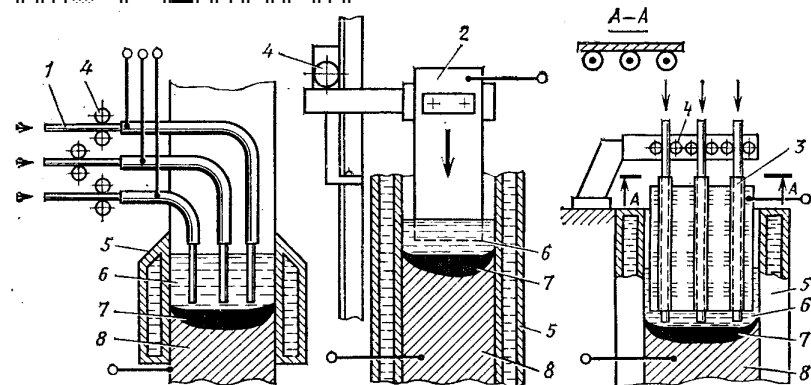
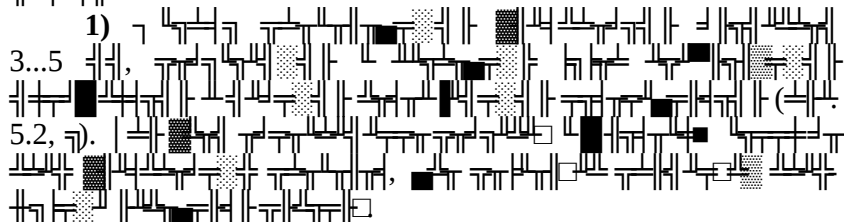
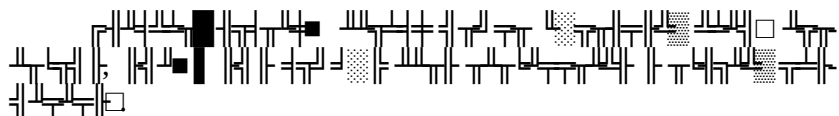
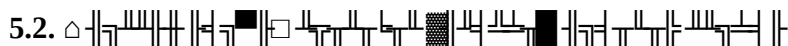
5.1.

;

γ 20 $\leq$ 50
 1949 $\cap \equiv$
 $\sqrt{\cdot}$
 1955
 35 $\tilde{n}$ 60
 1900-2000° $\gamma \cdot f$
 20 $\tilde{n}$ 3000



5.1.



60, 200. $\approx$
 V_1 ,
 2,5.

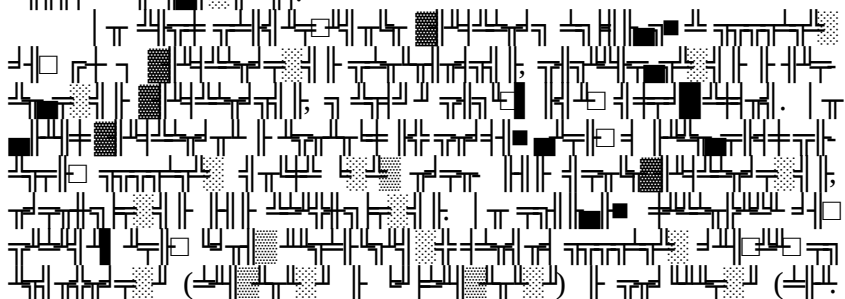
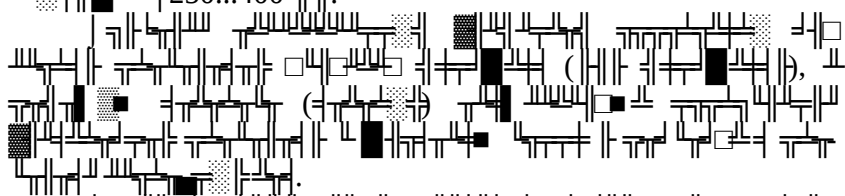
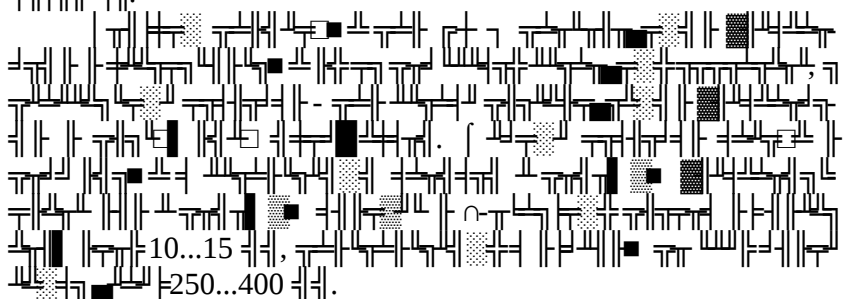
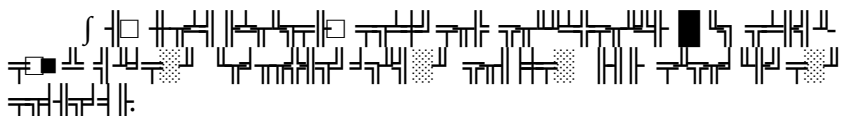
2) (5.2, 5).
 1...1,2 10...12
 200, 800, V_1 1,2...3,5/

∞

3) (5.2, 5).
 3
 500, 1000, 1500

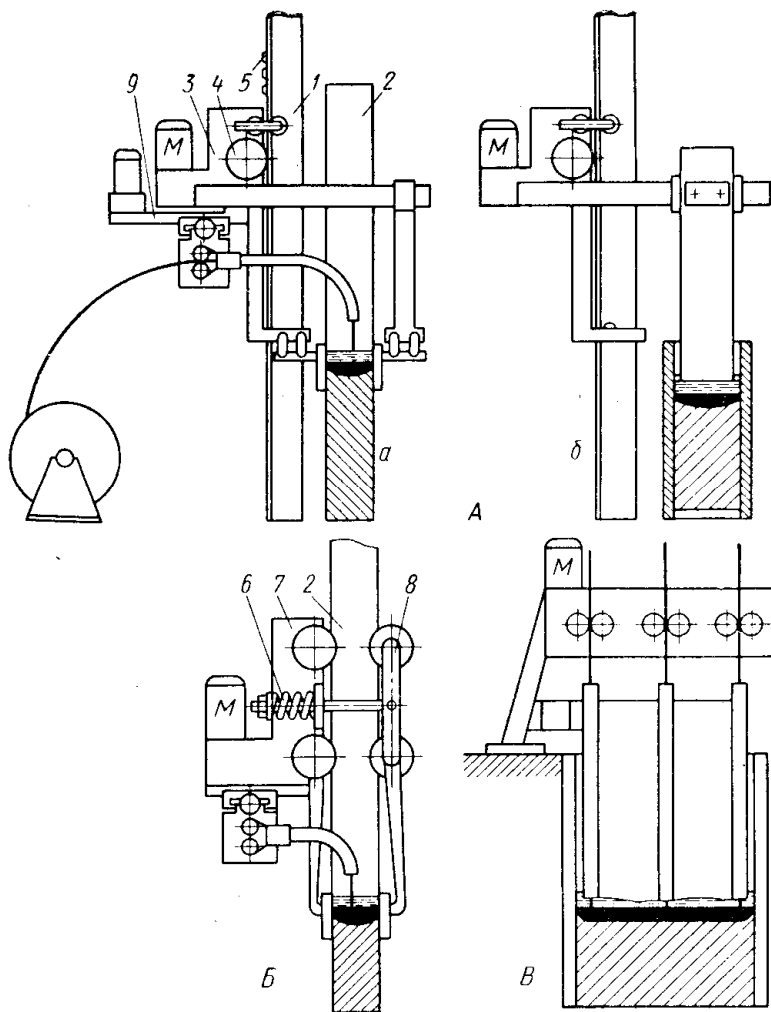


5.3. —

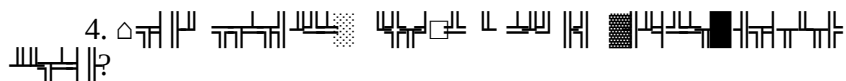


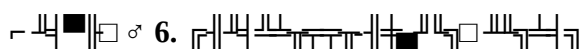
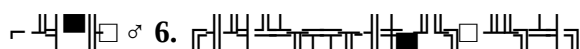
5.3).

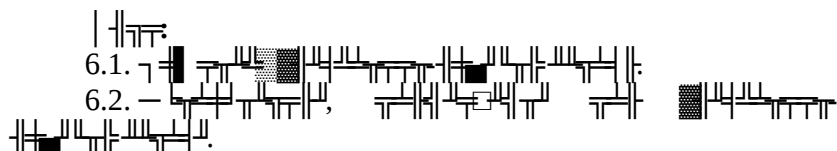
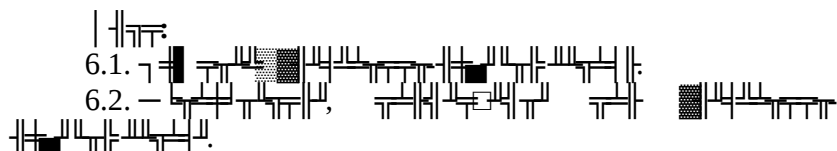
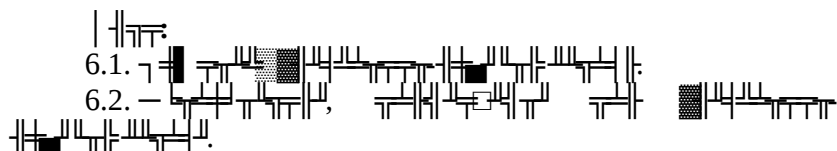


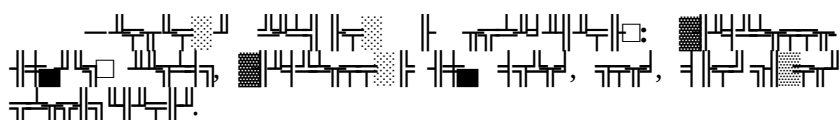


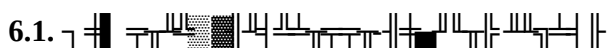
5.3. $\sqrt{\tilde{n}}$ $\infty \tilde{n}$ $\angle \tilde{n}$ (γ)
 (b) $1 \tilde{n}$ $2 \tilde{n}$ $3, 7 \tilde{n}$ $8 \tilde{n}$
 $4 \tilde{n}$ $5 \tilde{n}$ $6 \tilde{n}$

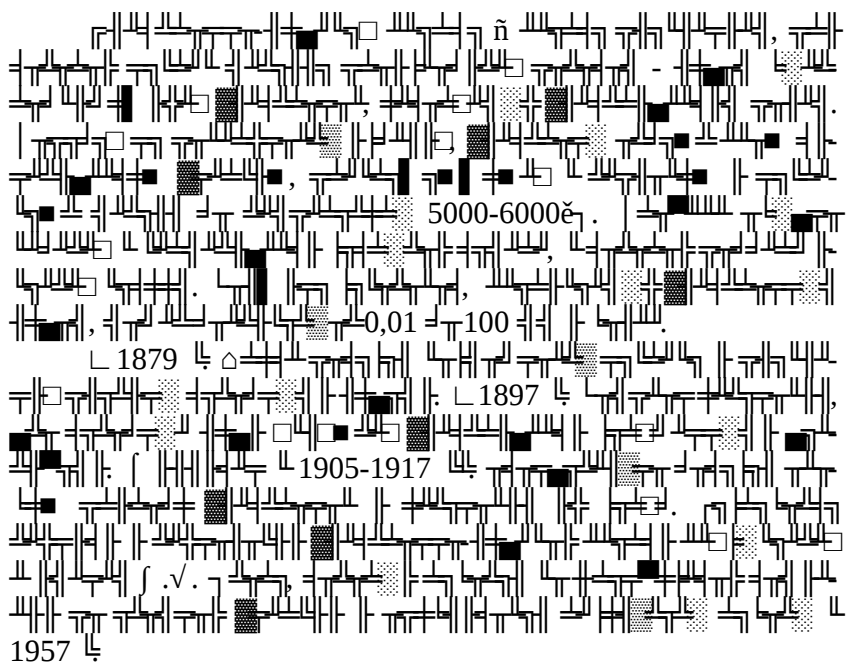
4. $\triangle$ 

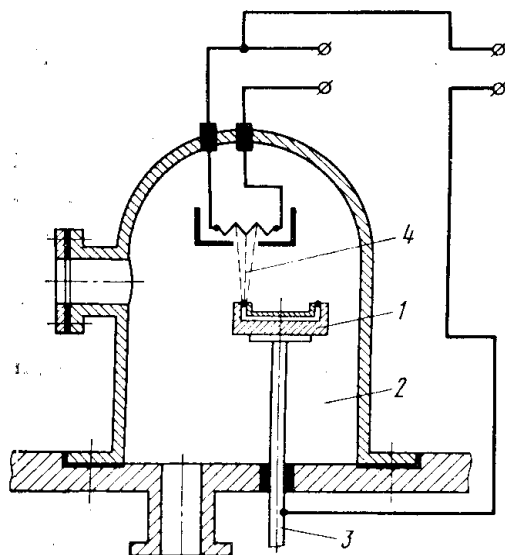
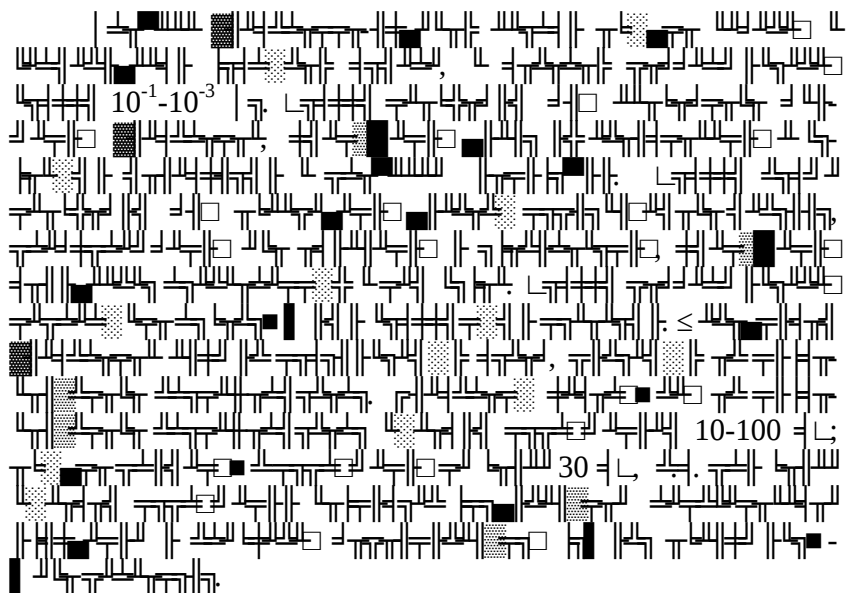
 6. 


 6.1. 
 6.2. 



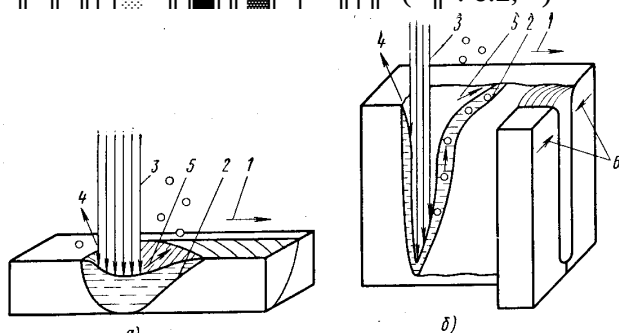
6.1. 


 5000-6000ě .
 0,01 100
 1879 1897
 1905-1917
 1957



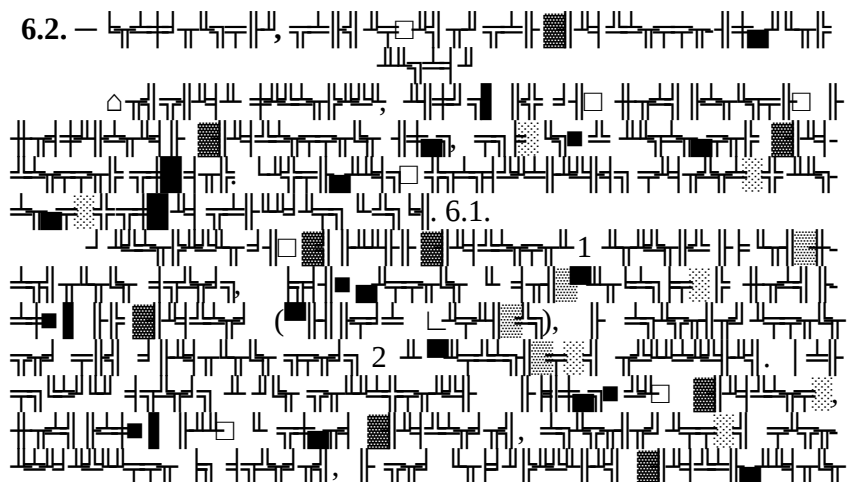
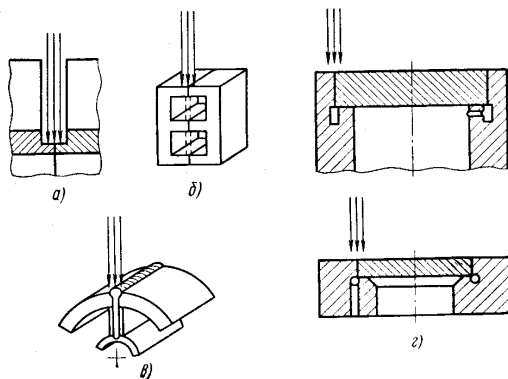
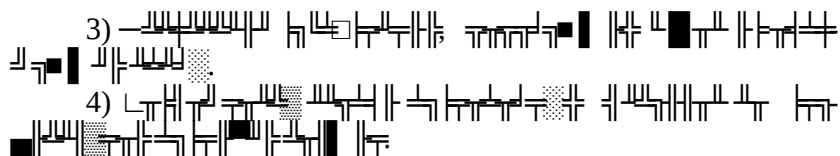
6.1. 1 - $\tilde{n}$; 2 - $\tilde{n}$; 3 - $\tilde{n}$; 4 - $\tilde{n}$

99%
(s Ô 1 ñ 3 ñ)
(. 6.2, ã).
(. 6.2, ß)



6.2. (ã)
(ß)
1 ñ 2 ñ 3 ñ 4 ñ 5 ñ 6 ñ

1) f
2)
26:1.



	-100	-101	-101-01	-858
	60	12	12	120
	1	0,8-1	-	1
	1	0,25	0,002	1
	60	3	0,18	120

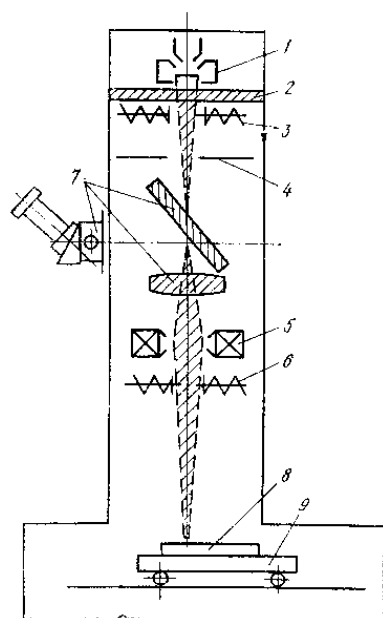
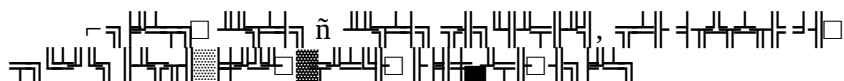
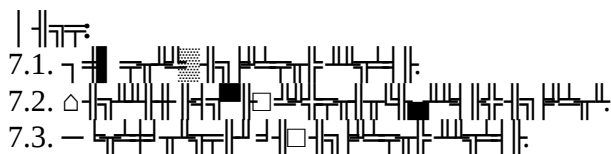
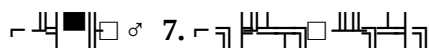
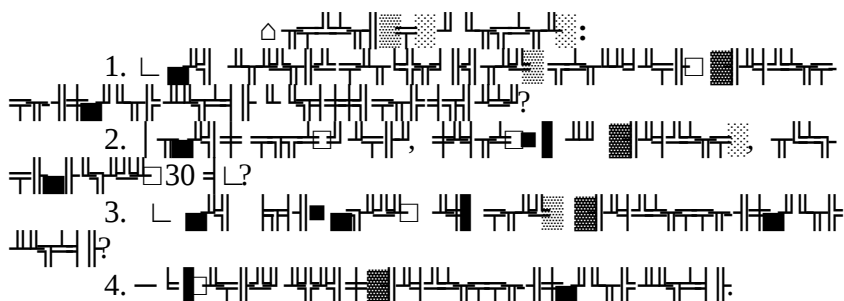
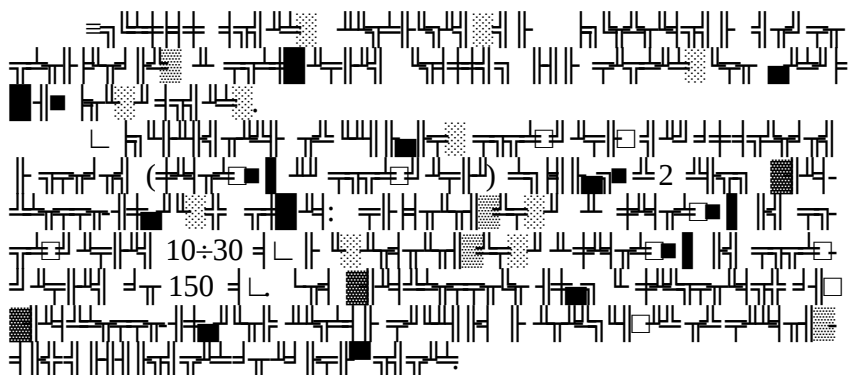


Рис. 6.4.

1 — объектив; 2 — предметный столик; 3 — конденсор;
4 — окуляр; 5 — объектив; 6 — предметный столик;
7 — зеркало; 8 — основание; 9 — платформа.



$\frac{1}{\sqrt{2}}$ 60- 20
 1962 1964 ñ 1966

$\frac{1}{\sqrt{2}}$ 60- 20
 1962 1964 ñ 1966

$\frac{1}{\sqrt{2}}$ 60- 20
 1962 1964 ñ 1966

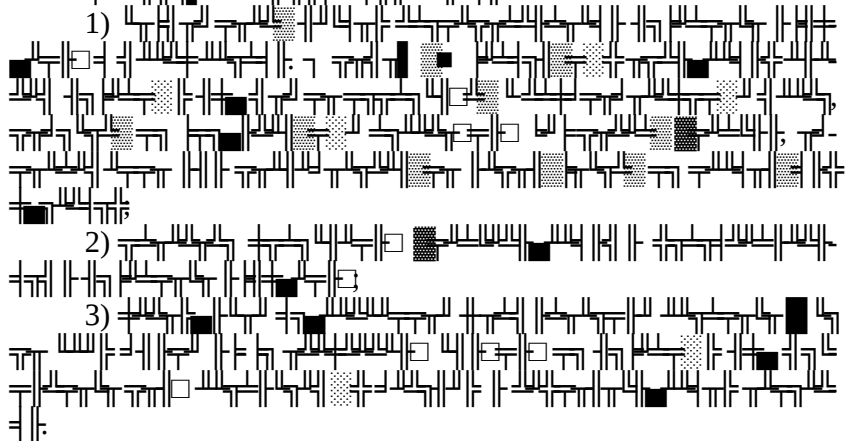
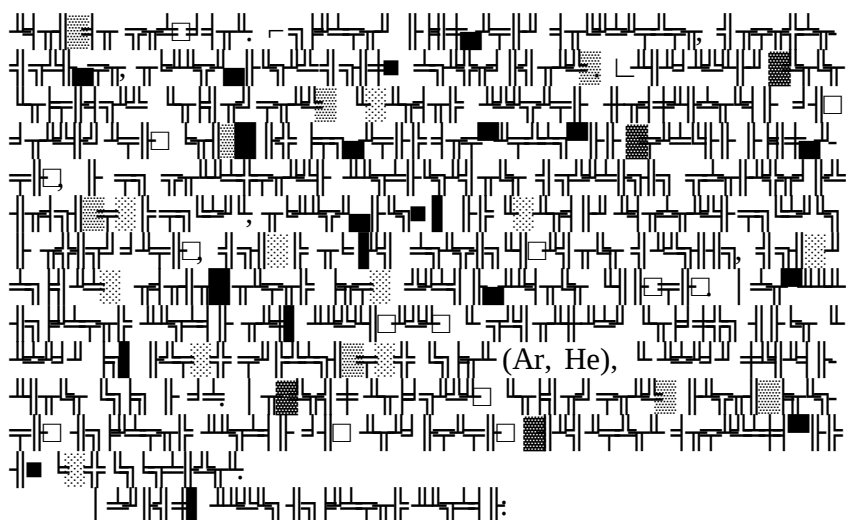
$\frac{1}{\sqrt{2}}$ 60- 20
 1962 1964 ñ 1966

$\frac{1}{\sqrt{2}}$ 60- 20
 1962 1964 ñ 1966

$\frac{1}{\sqrt{2}}$ 60- 20
 1962 1964 ñ 1966

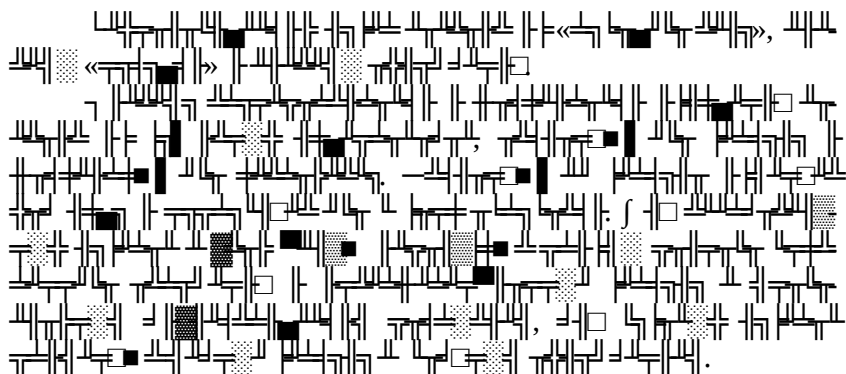
$\frac{1}{\sqrt{2}}$ 60- 20
 1962 1964 ñ 1966

$\frac{1}{\sqrt{2}}$ 60- 20
 1962 1964 ñ 1966

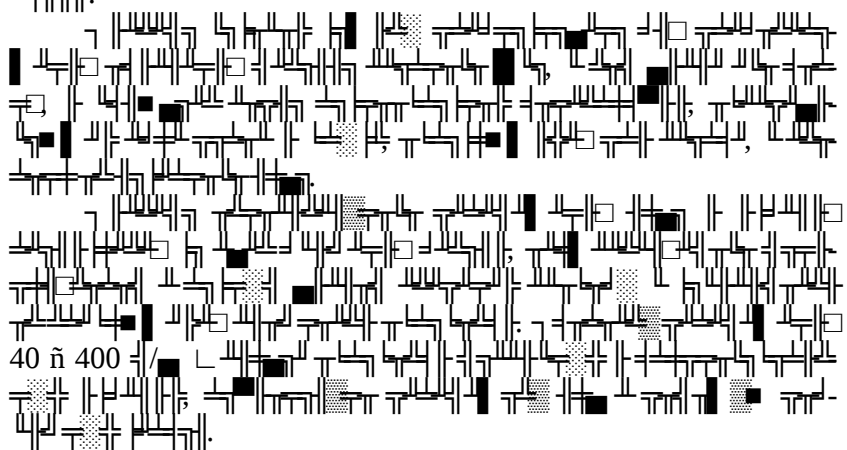


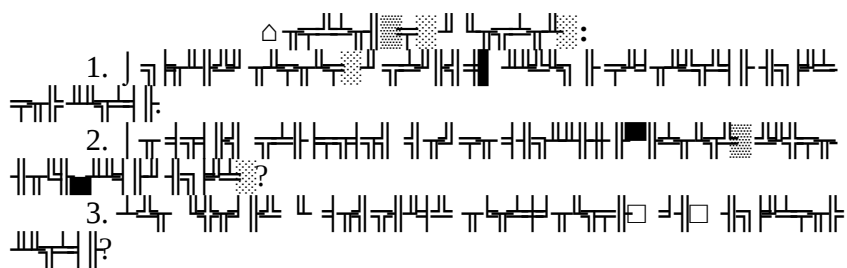
7.2. $\triangle$

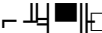




7.1. 

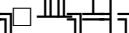


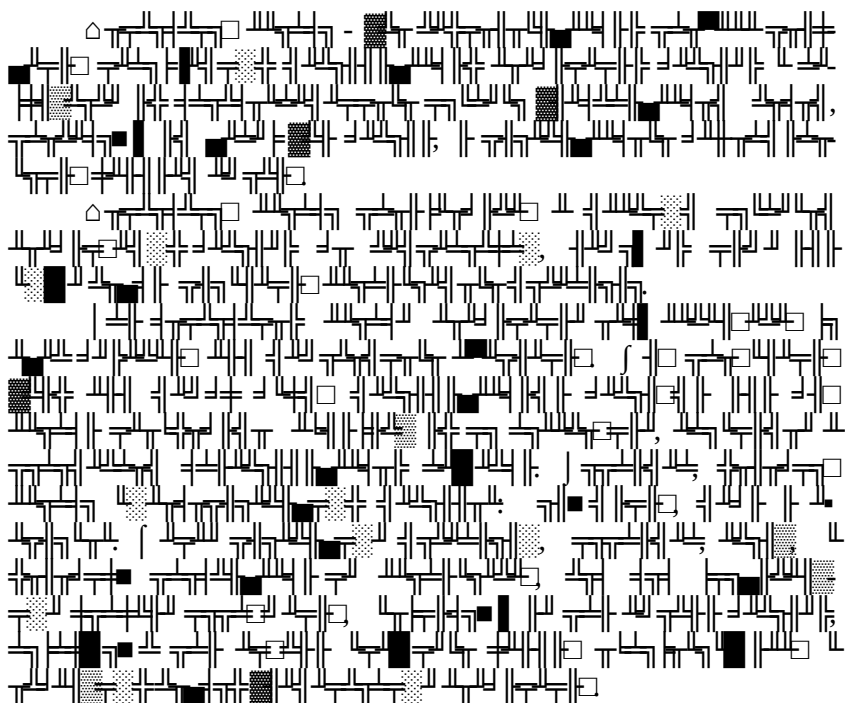


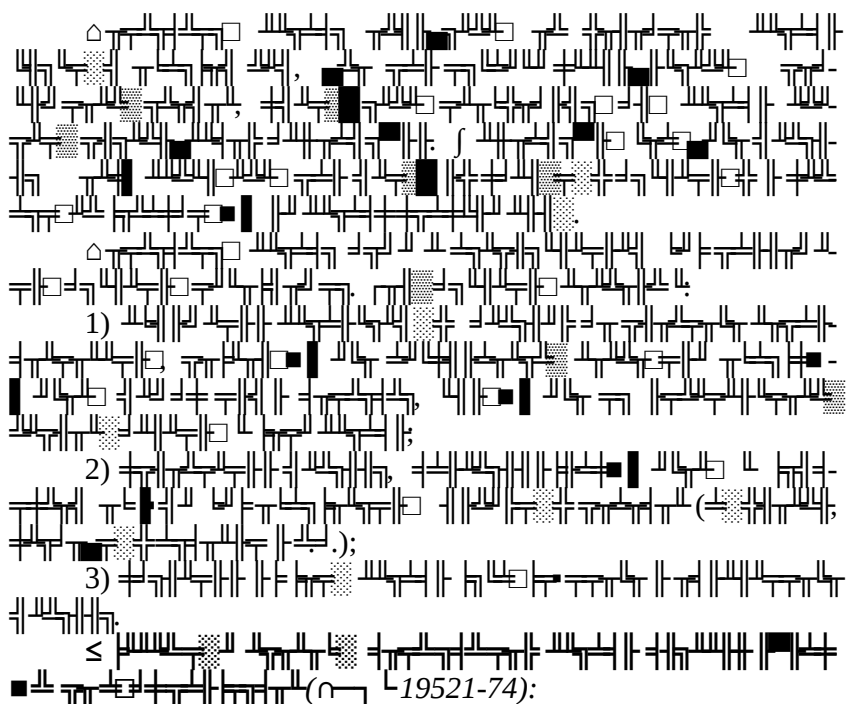
8.  8. 

- 8.1. 
 8.2. 
 8.3. 
 8.4. 
 8.3. 



8.1.  8.1. 





1) $\leq$

- $\leq$
 - $\leq$
 - $\leq$
 - $\leq$

2) $\leq$

- $\leq$
 - $\leq$

3) $\leq$

- $\leq$
 - $\leq$

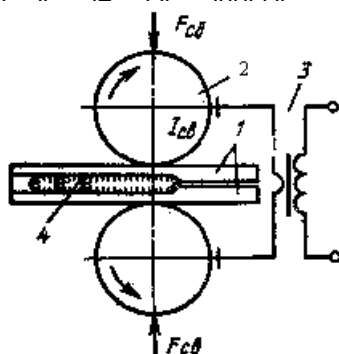
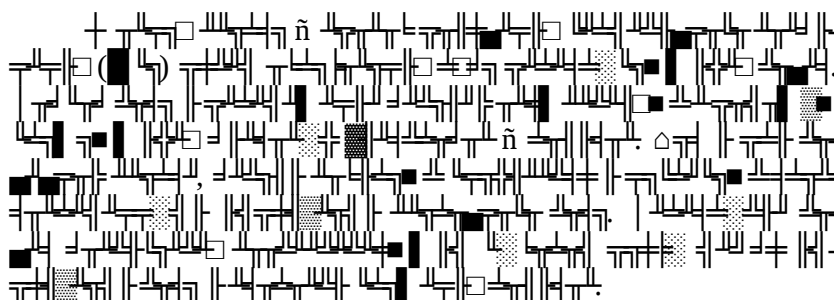
3) $\leq$

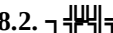
- $\leq$
 - $\leq$

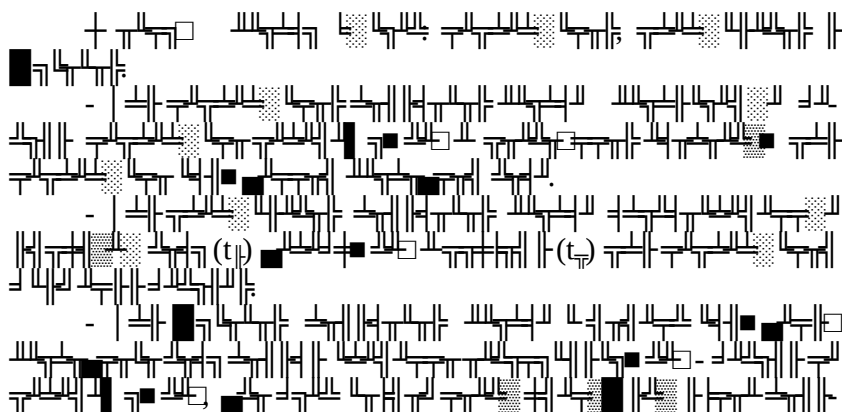
4) $\leq$

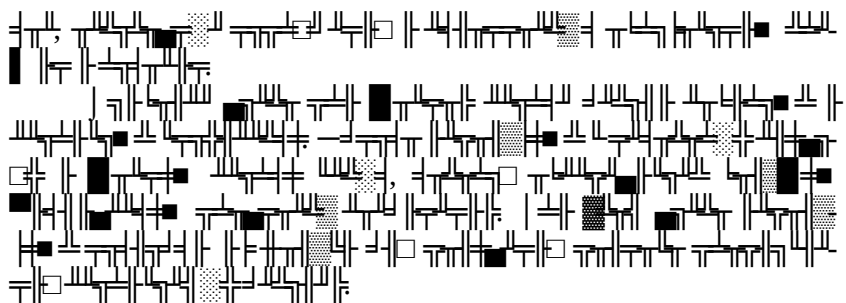
- $\leq$

8.3.

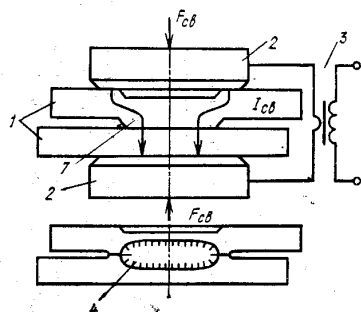


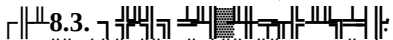
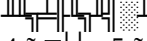
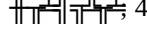
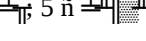
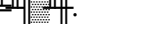
8.2.  1  2  3  4 

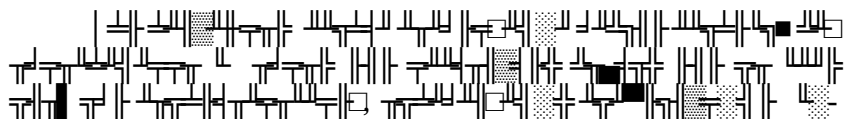




8.4.



8.3.  1  2  3 
 4  5 .





8.5.



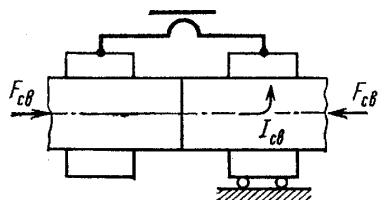
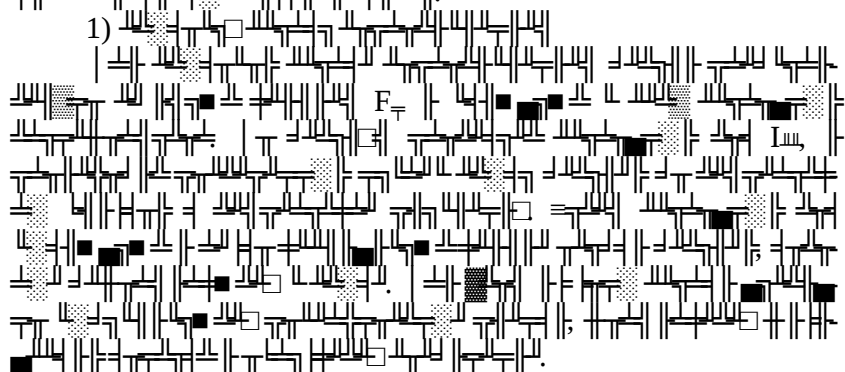
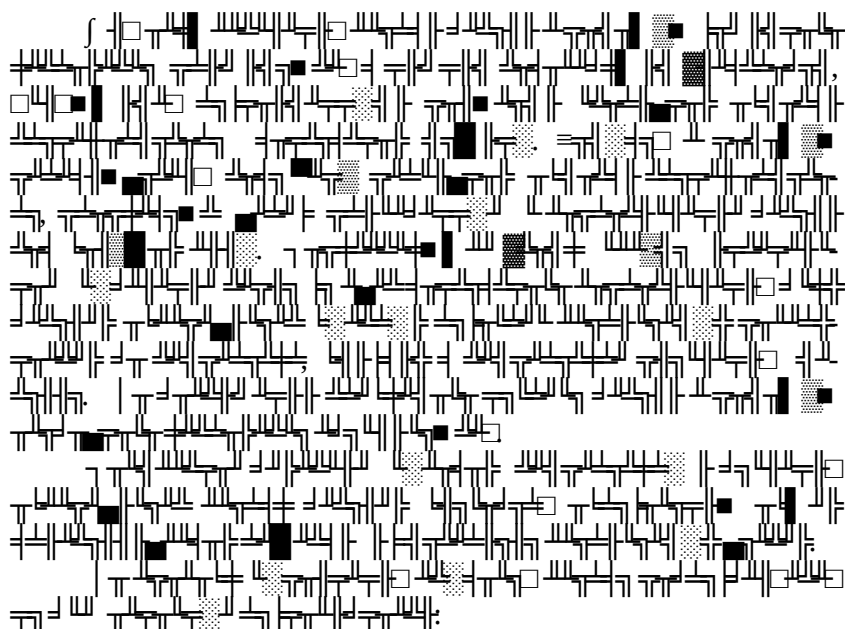
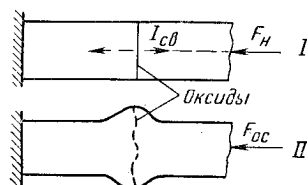
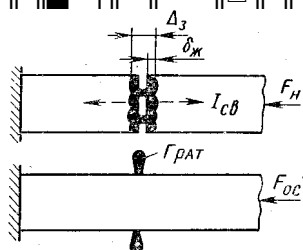
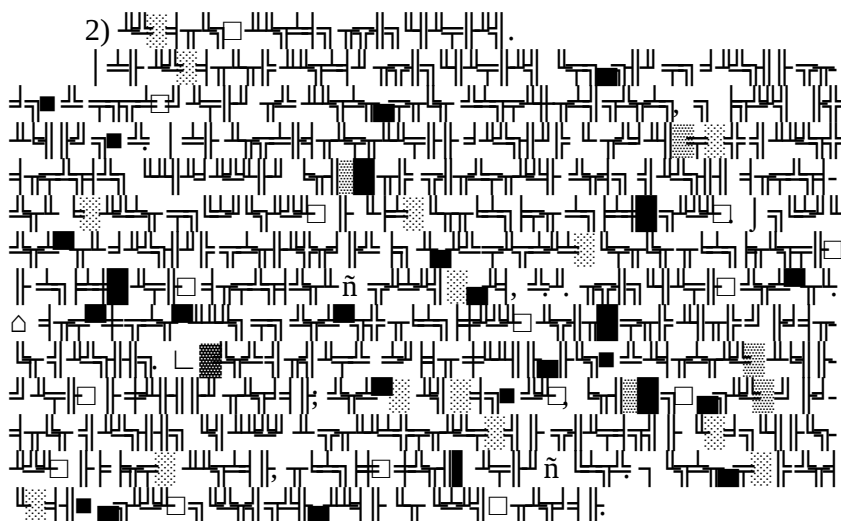


Fig. 8.4.





8.5. $(F_{\tau} \tilde{n}$; $F_{\tau} \tilde{n}$).

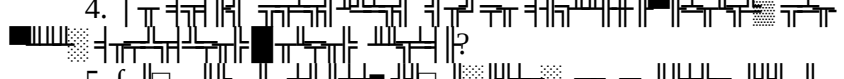


8.6. $(F_{\tau} \tilde{n}$; $F_{\tau} \tilde{n}$; Δ_3 - $\delta_{\parallel}$).

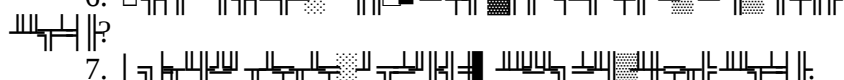
1. 

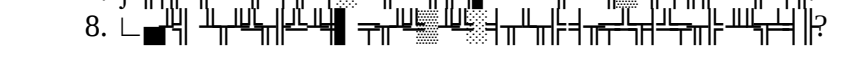
2. 

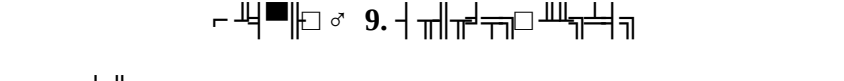
3. 

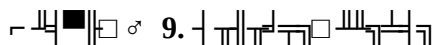
4. 

5. 

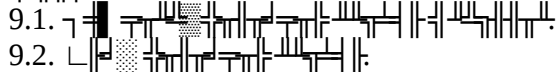
6. 

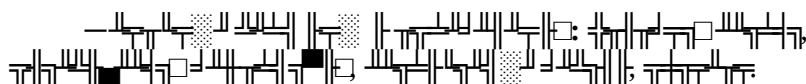
7. 

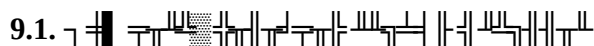
8. 

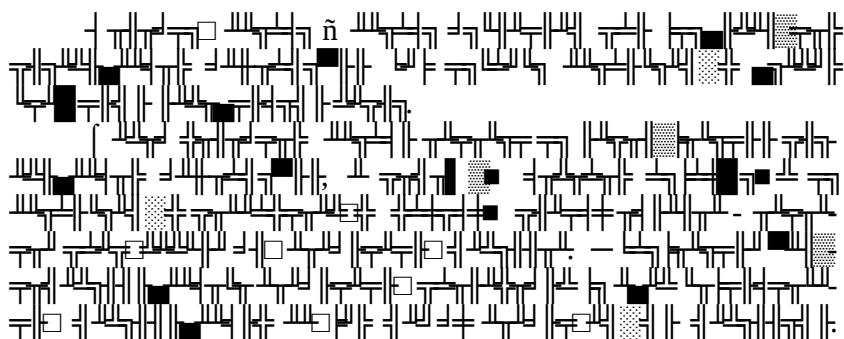


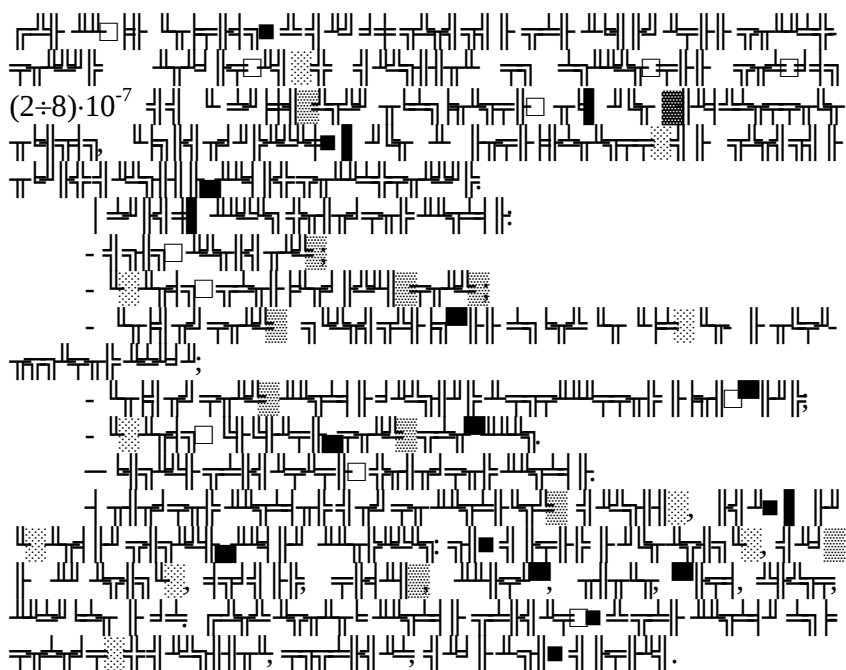
9.1. 

9.2. 

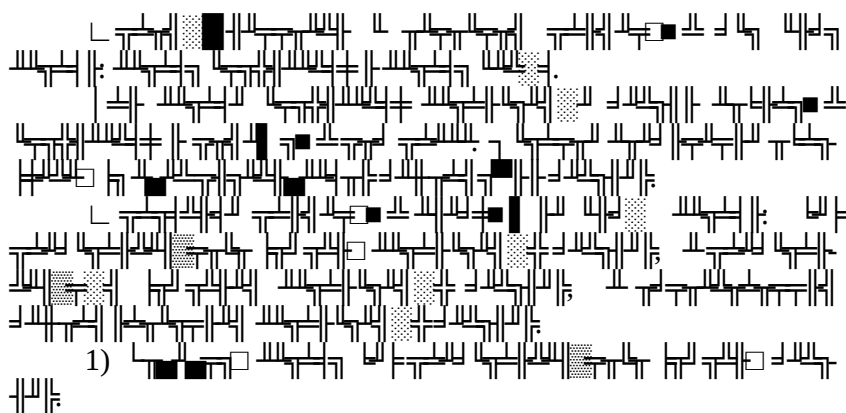


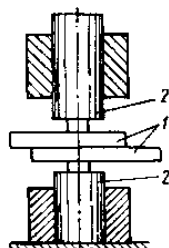
9.1. 





9.2.

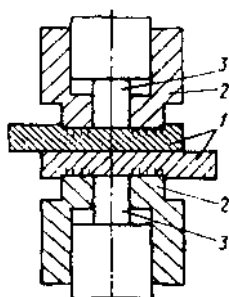




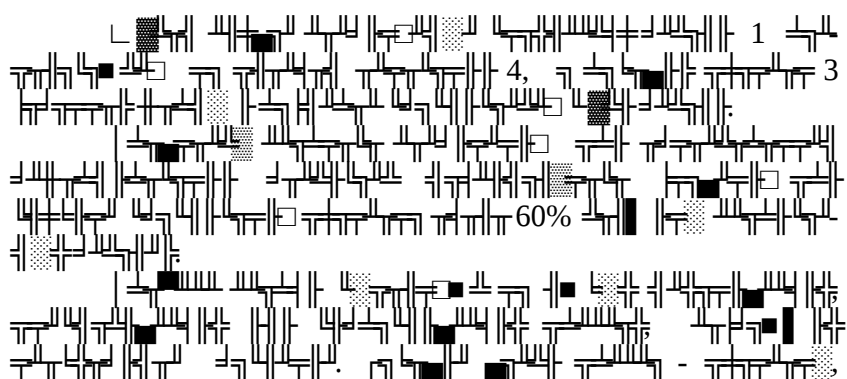
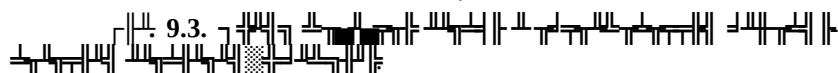
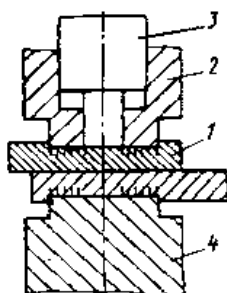
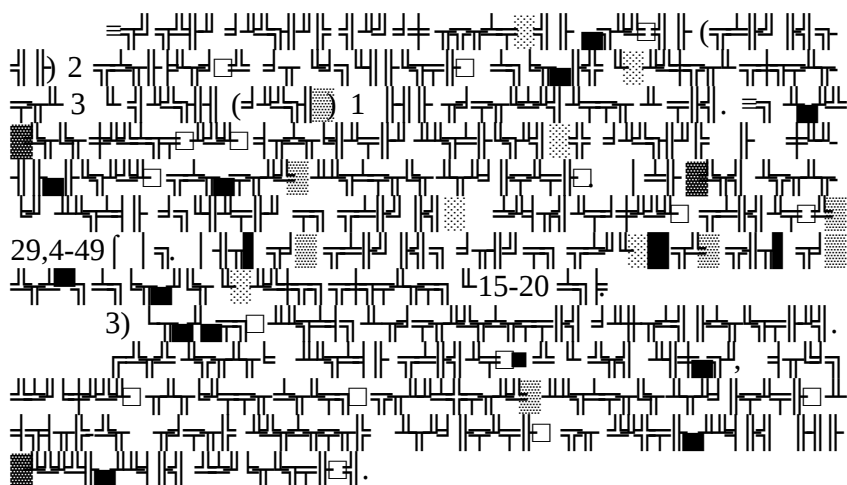
9.1.

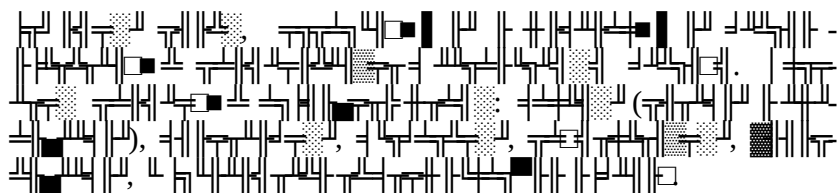
1, 2. 1-3

2)



9.2.





1. $\angle$?

2. $\int$:

3. $\triangle$?

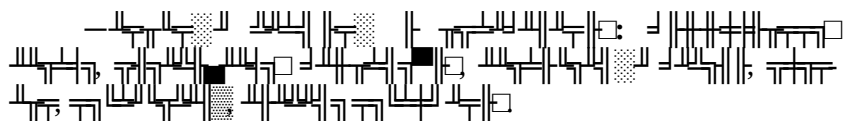
4. $\angle$?

5. $\triangle$?

$\angle$ σ 10. $\int$ $\square$ $\square$

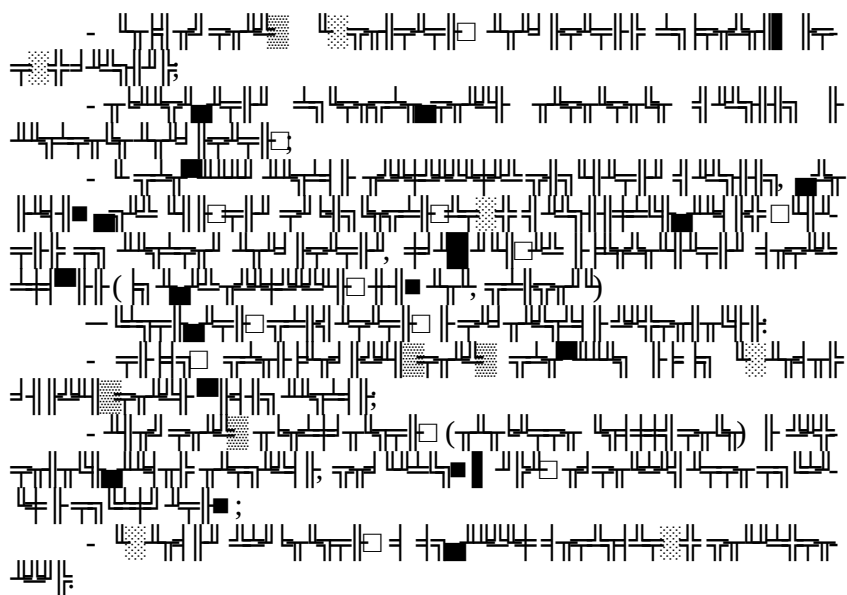
10.1. $\angle$:

10.2. $\angle$:



10.1. $\angle$ $\int$ $\square$ $\square$

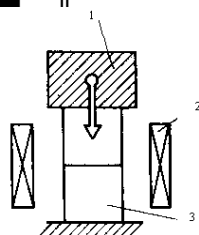




10.2.



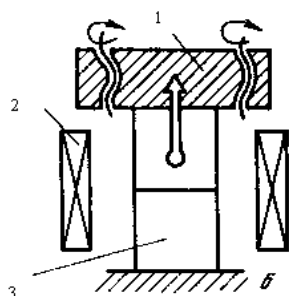
1) $\int$



 10.1.        

1- 2 ñ 3 ñ

2)



10.2. 1 ñ 2 ñ 3 ñ

1. 2. 3.

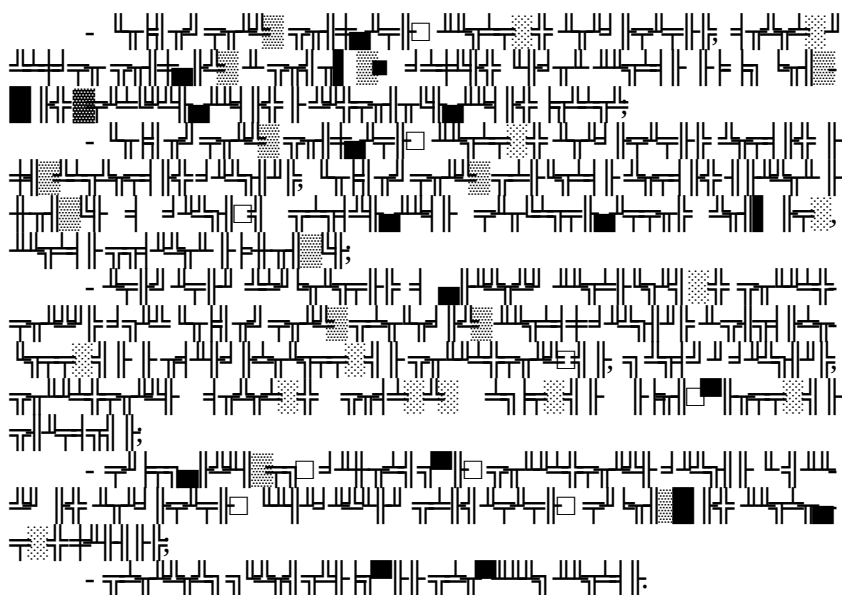
11.

11.1. 11.2.

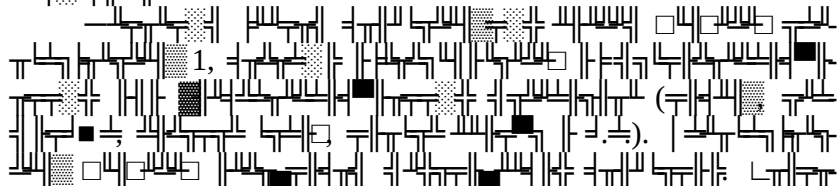
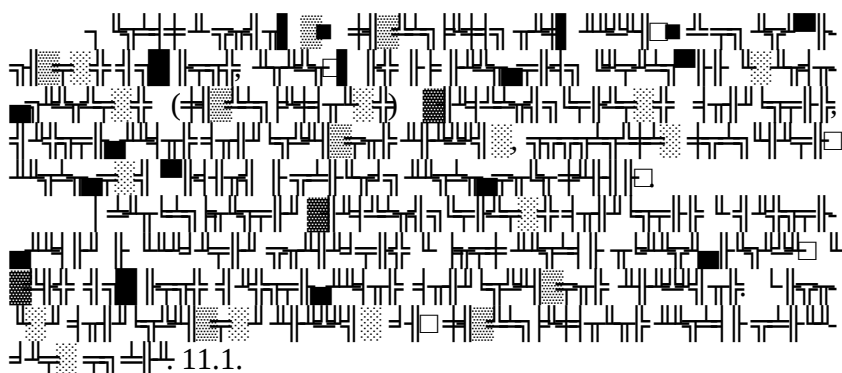


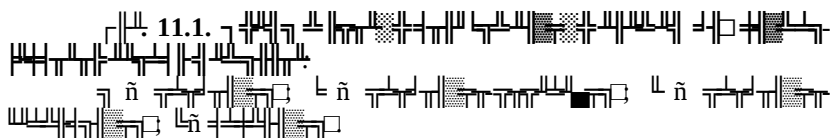
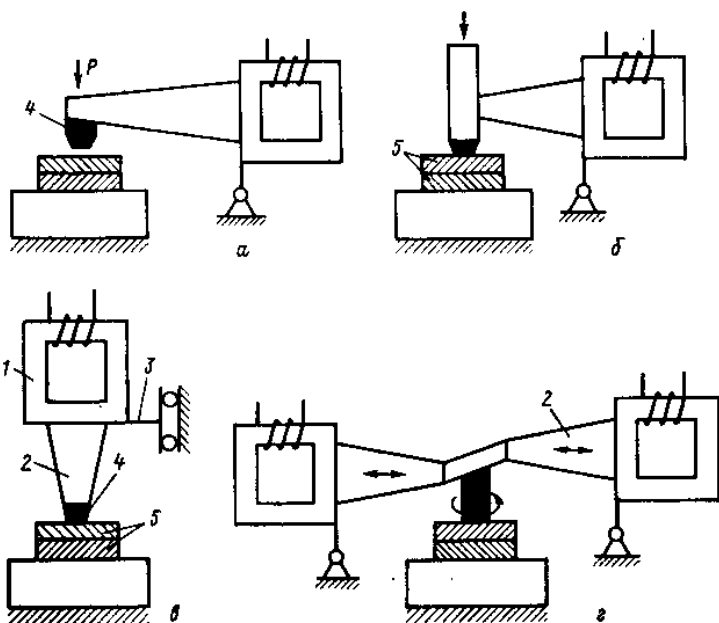
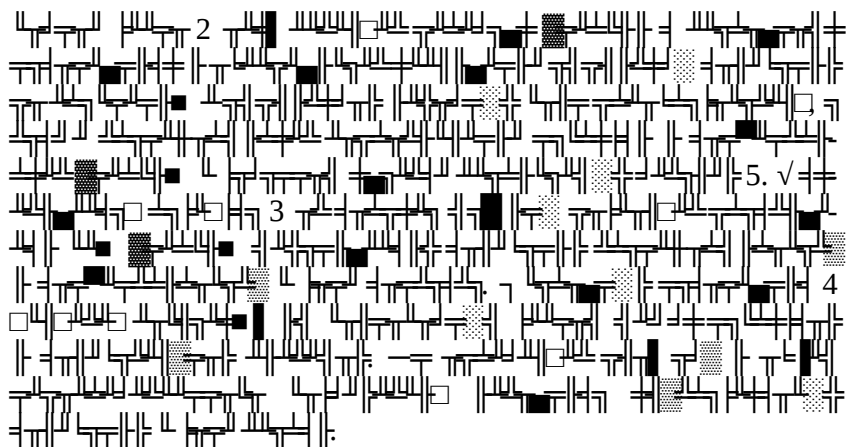
11.1.

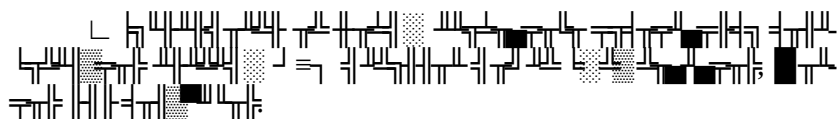




11.2. —







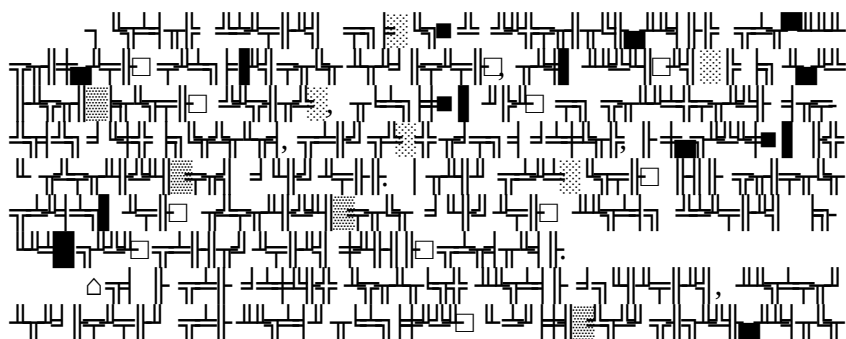
1. ?
2. ?
3. ?
4. ?

12. ♀

- 12.1. .
- 12.2. .



12.1. ♀



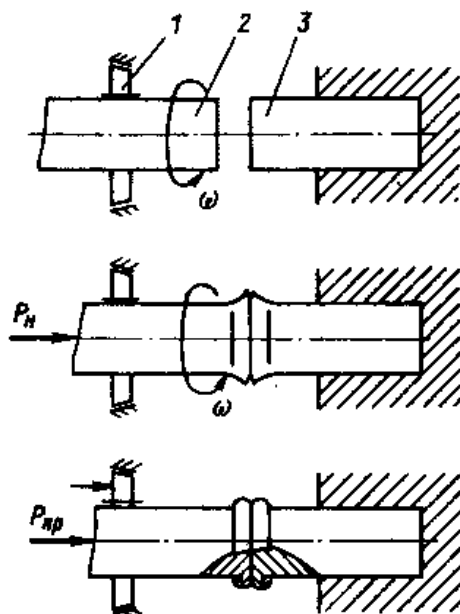
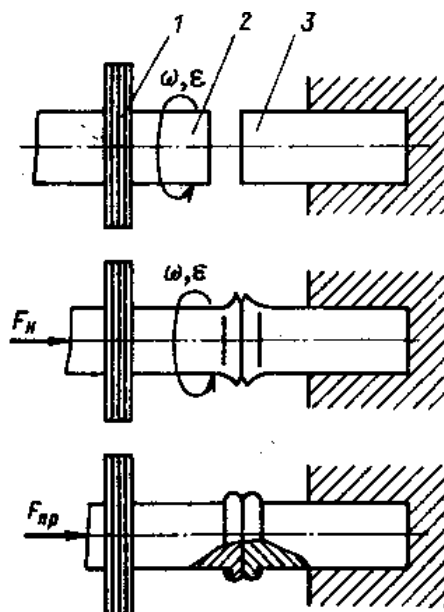


Рис. 12.1. 1 - штифт; 2, 3 - опора:

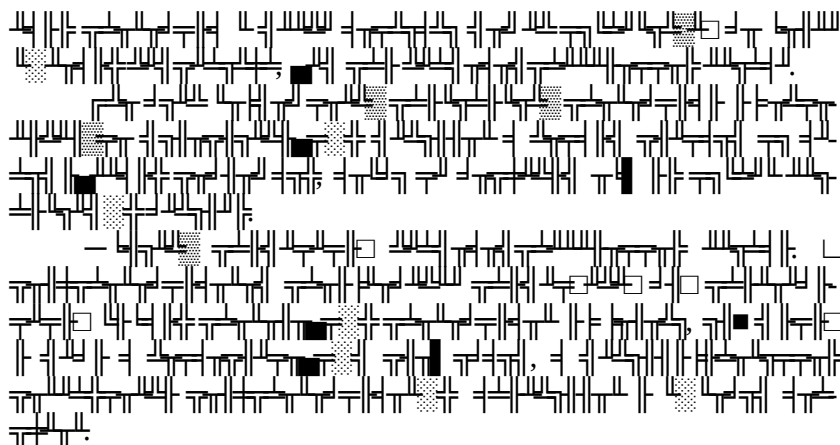
2) ≤ $\frac{P_H}{P_T}$; $\frac{P_H}{P_T}$ — коэффициент, зависящий от угла наклона α и от коэффициента трения μ . При $\alpha = 0$ и $\mu = 0$ коэффициент равен 1. При $\alpha = 0$ и $\mu = 1$ коэффициент равен 2. При $\alpha = 45^\circ$ и $\mu = 0$ коэффициент равен 1. При $\alpha = 45^\circ$ и $\mu = 1$ коэффициент равен 2.



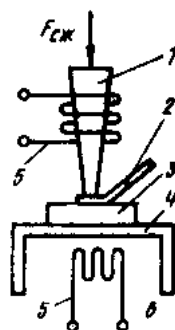
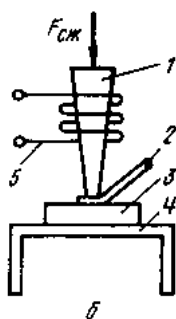
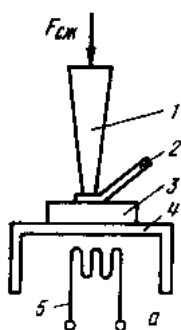
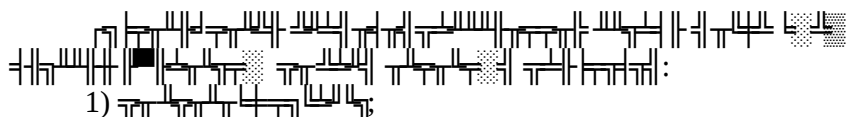
12.2. 1- ; 2,3 ñ

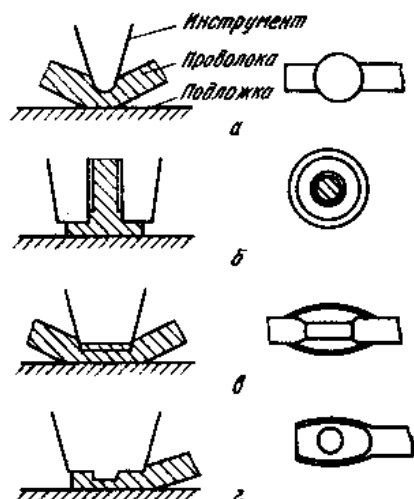
3) Δ ω , $n = 5-6$

1. Δ ?
 2. Δ ?
 3. Δ ?



13.2.



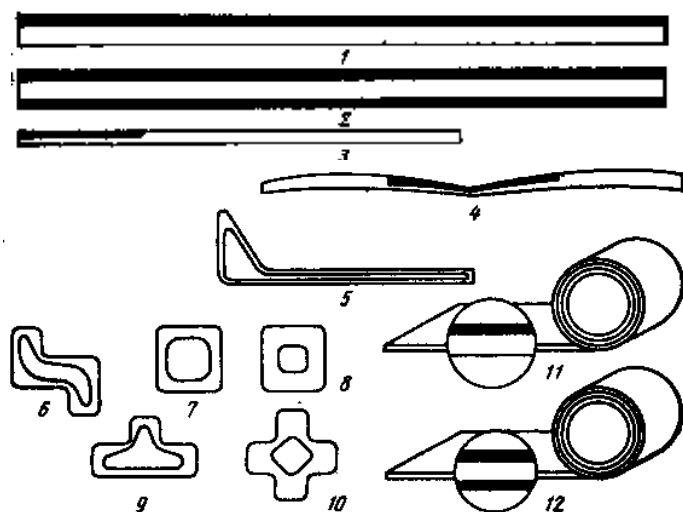


13.3. (Technical drawing of a wire welding process showing a cross-section of a wire being welded to a base metal.)

13.3. (Technical drawing of a wire welding process showing a cross-section of a wire being welded to a base metal.)

(Technical drawing of a wire welding process showing a cross-section of a wire being welded to a base metal.)

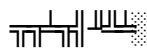
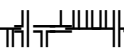
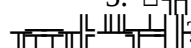
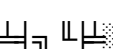
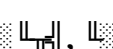
13.5.

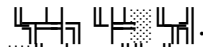


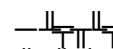
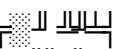
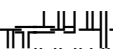
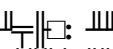
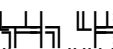
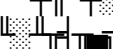
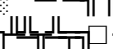
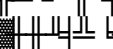
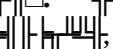
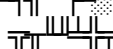
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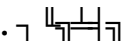
1 ñ 2 - 3 ñ 4 ñ 5-10 - 11 - Fe-Ni; 12 ñ Al-Fe-Ni.

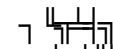
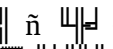
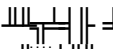
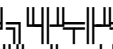
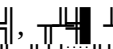
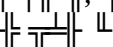
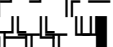
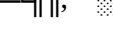
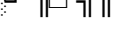
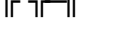
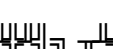
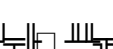
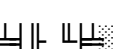
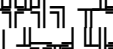
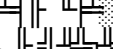
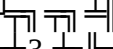
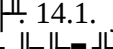
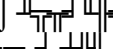
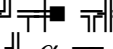
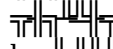
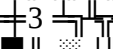
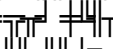
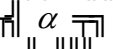
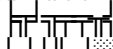
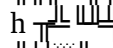
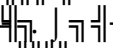
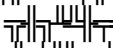
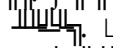
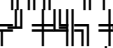
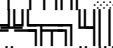
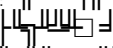
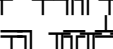
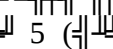
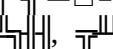
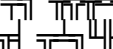
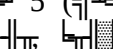
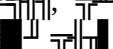
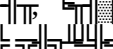
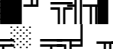
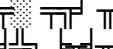
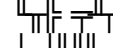
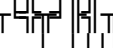
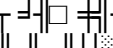
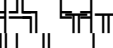
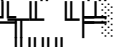
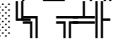
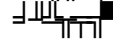
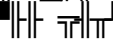
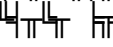
1. 2. 3. 4.

5. $\triangle$      
  σ 14.     


 14.1. .
 14.2. .
 14.3. .

14.1. 

   $\hat{n}$    
       
       
       
       
       
       
       
       
       
       
       
       
       
       



$\alpha = 0.$
 D
 V_0
 $\gamma = \alpha + \beta.$
 $V_4,$
 γ
 $10^{-6} \tilde{n} 10^{-5}$

$$W = \frac{m_1 m_2}{2(m_1 + m_2)} v_0^2 \left[1 - \left(\frac{v_{\perp}}{v_0} \right)^2 \right],$$

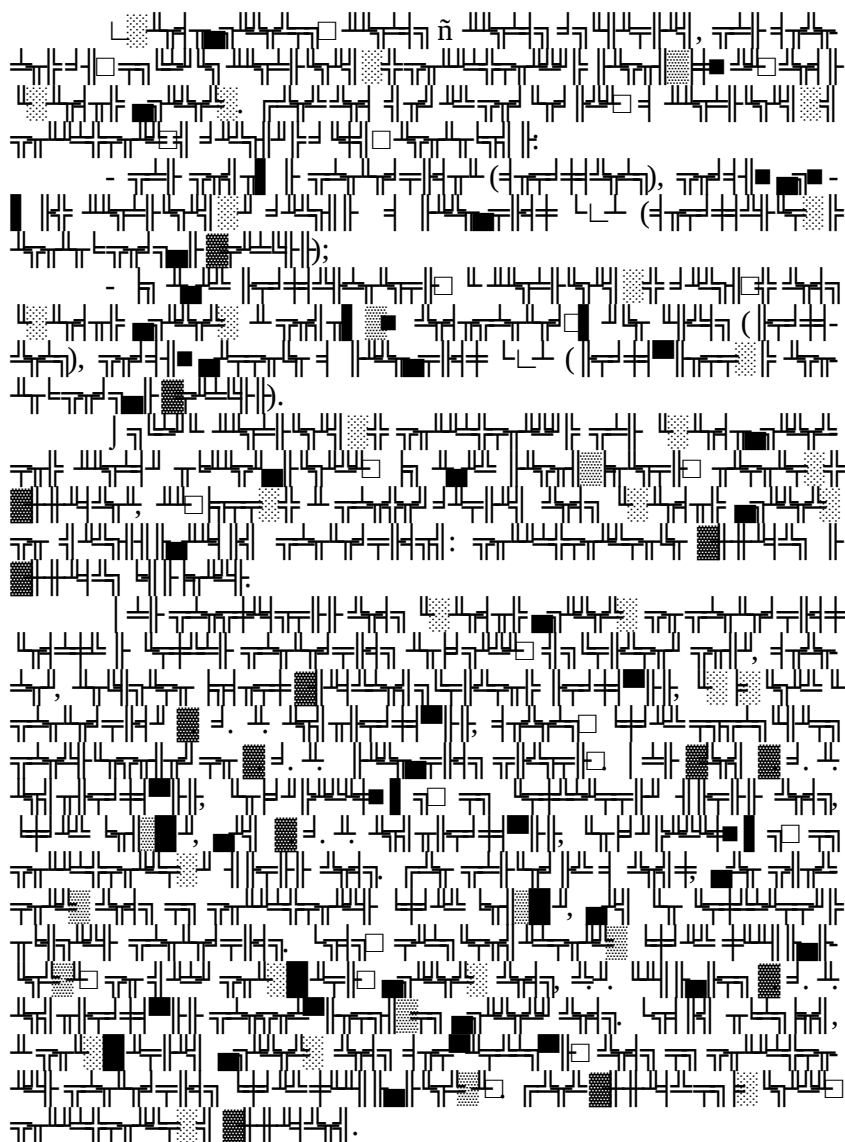
$$v_{\perp} = D \sin(\gamma - \alpha) / \sin \gamma,$$

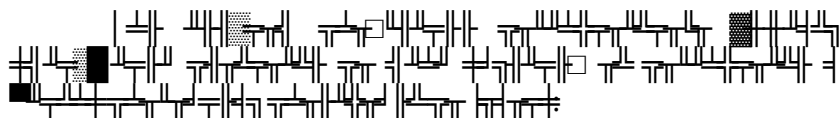
$$\gamma = \alpha + \beta = \alpha + 2 \arcsin(v_0 / 2D).$$

$$v_{\perp} = D,$$

$$\gamma = 2 \arcsin(v_0 / 2D).$$

14.2.



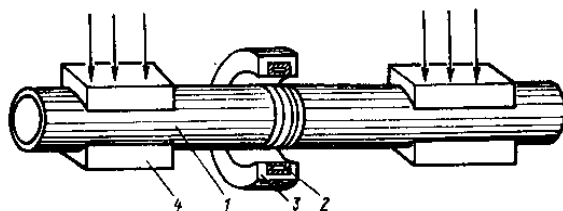
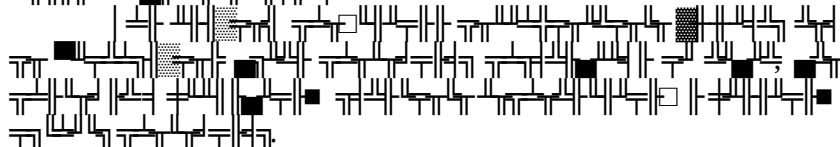


$$I_x = I_0 e^{-x/\Delta},$$

I_x - Δ - $\Delta = 503 \sqrt{\rho / \mu f}$, ρ - 20° , μ - f

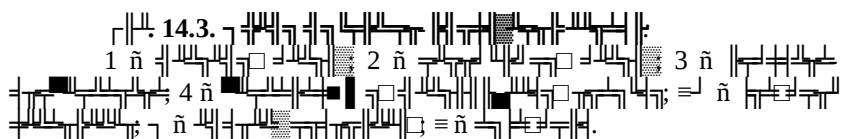
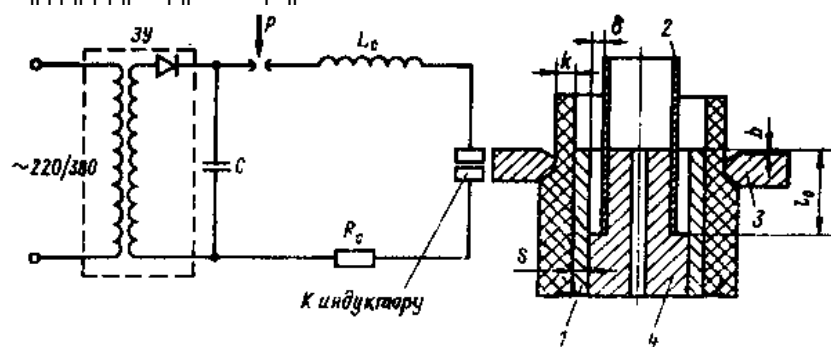
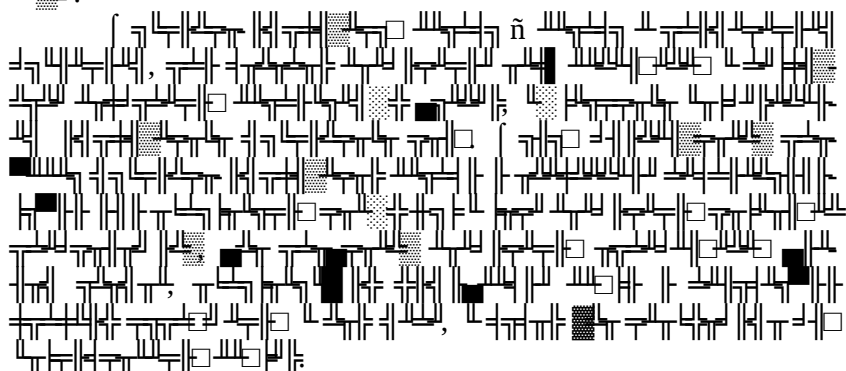
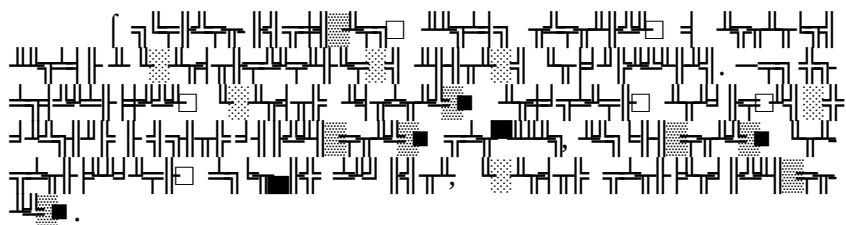
$$\Delta = 503 \sqrt{\rho / \mu f},$$

ρ - 20° , μ - f



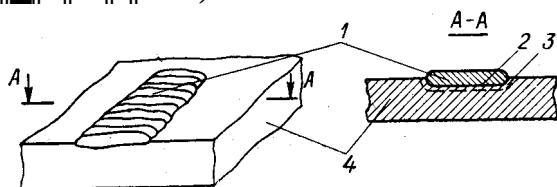
14.2. 1 - 2 - 3 - 4

14.3.

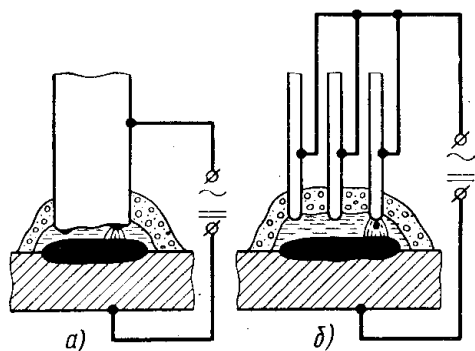
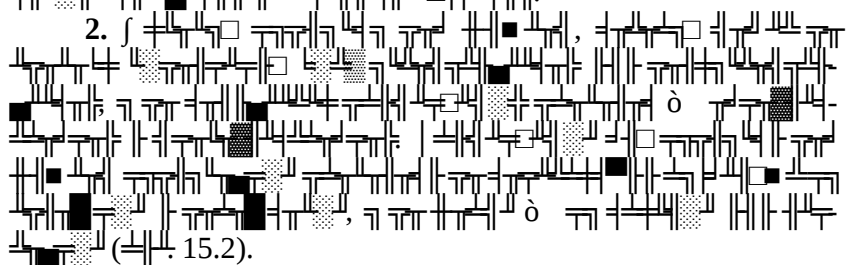
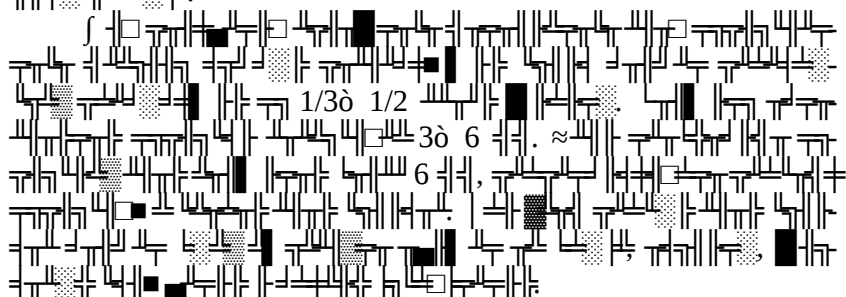
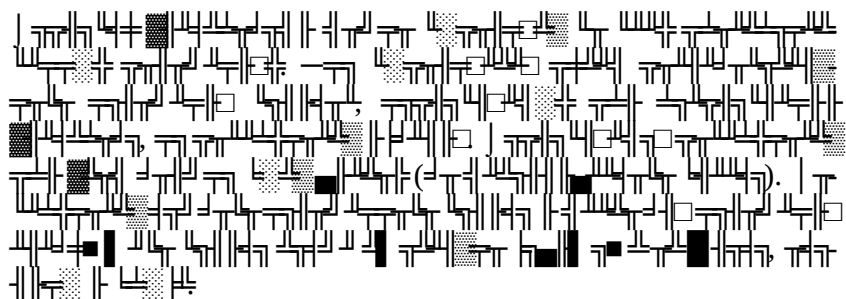


15.2.

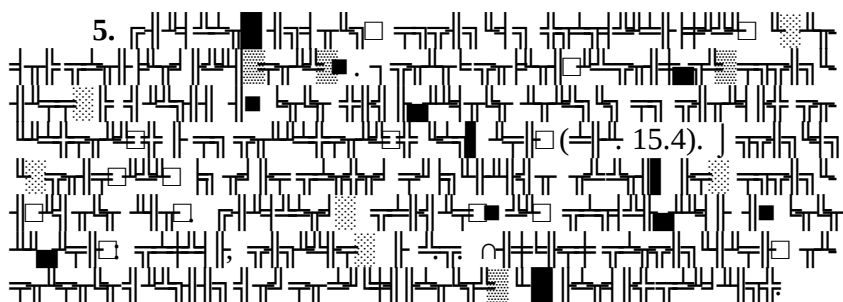
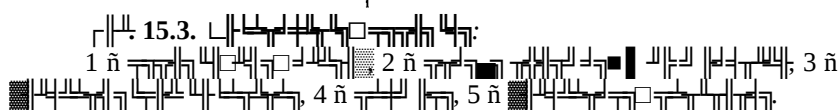
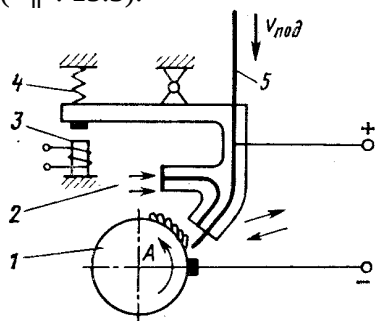
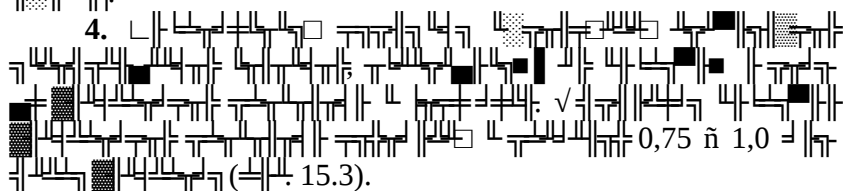
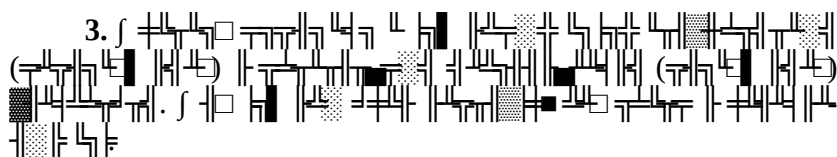
16.1.

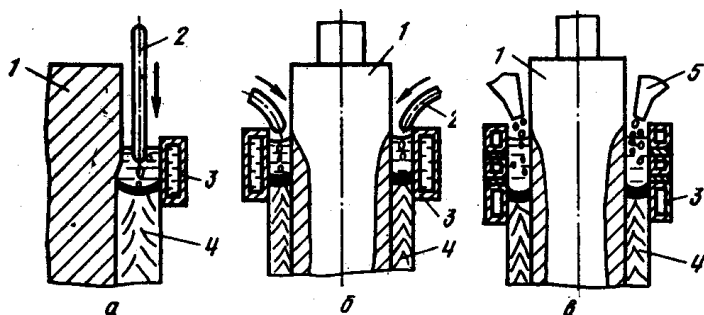


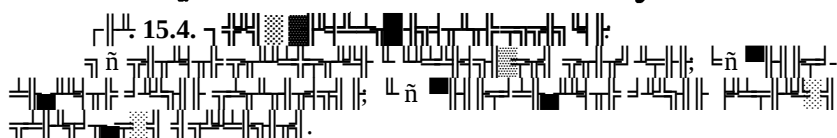
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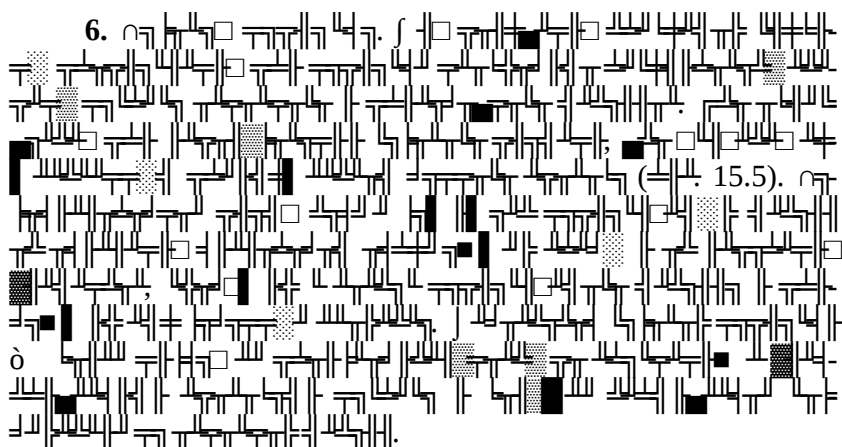
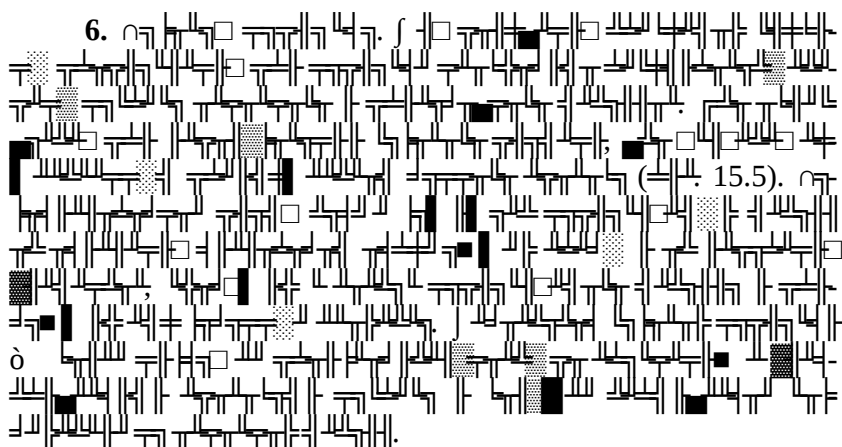


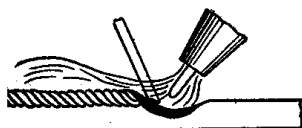
15.2.

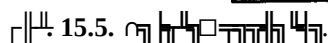




15.4. 

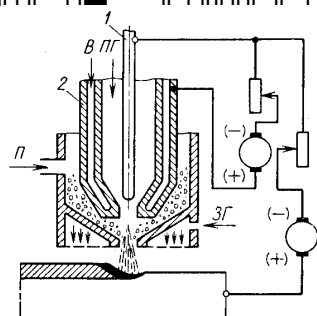
6.  (15.5). 



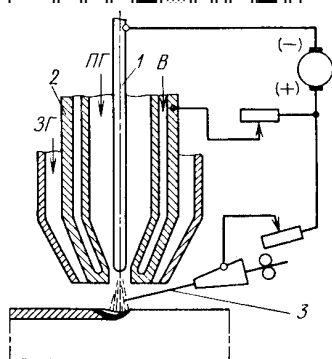
15.5. 

7. 

(15.6, 15.7).



15.6. 1 - катод; 2 - сетка; 3 - анод. B - магнитное поле.



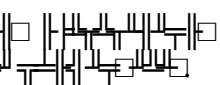
15.7. 1 - катод; 2 - сетка; 3 - анод. B - магнитное поле.

15.1).

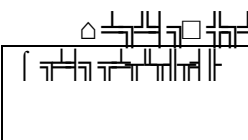
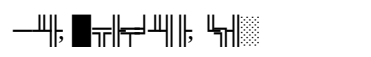
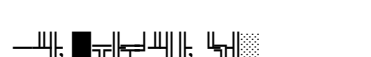
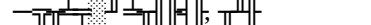
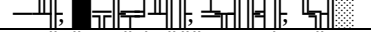
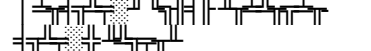
15.1

	$\frac{4}{4}$
	0,8 - 3
	2 - 12
	5 - 40
	5 - 40
	1,5 - 9,0
	1,0 - 7,0
	1,2 ñ 3
	20 - 60
	20-200
	0,8 ñ 12
	2 - 12

15.2.


 $\equiv$ | $\overline{\text{tr}} \equiv 0$ | $\cap \sqrt{}$, $\cap$ L 10543 δ 98. $\int$ 

 15.2

		
$\int \overline{\text{tr}} 25$ $\overline{\text{tr}} 30$	160-220	
$\int \overline{\text{tr}} 35$ $\int \overline{\text{tr}} 40$ $\int \overline{\text{tr}} 45$	170-230	
$\int \overline{\text{tr}} 50$	180-240	
$\int \overline{\text{tr}} 65$	220-300	
$\int \overline{\text{tr}} 80$	260-340	
$\int \overline{\text{tr}} 40 \cap$	180-240	
$\int \overline{\text{tr}} 50 \cap$	200-270	
$\int \overline{\text{tr}} 65 \cap$	230-310	
$\int \overline{\text{tr}} 10 \cap 3$	250-330	$\neq$ 
$\int \overline{\text{tr}} 30 \mid \cap \sqrt{}$	220-300	
$\int \overline{\text{tr}} 14 \cap$ $\int \overline{\text{tr}} 19 \cap$	240-260 300-310	
$\int \overline{\text{tr}} 30 \mid 5$	370-240	

0,25% 160 = 310 J L
 220δ 330 L 32δ 40 J R₇.
 180 = 280 J L 32 = 52
 J R₇, 10051δ 75
 44 25 = 65 J R₇.
 -5- 24- 12 -5δ
 24 12
 0,24%
 12%

$\vdash 10n2$ $\vdash 11n3$ $\vdash 12n4$ $\vdash 15n5$ $\vdash 30n2 \vdash$	$\equiv -250$ $\equiv -300$ $\equiv -350$ $\equiv -400$ $\vdash 70$	
$\vdash 16n2 \vdash$ $\vdash 35n6$ $\vdash 30 \vdash 8 \vdash 3$ $\vdash 35 \vdash 12 \vdash 3 \vdash$ $\vdash 90 \vdash 4 \vdash 4 \vdash$	$\equiv -1$ $\vdash -4$ $\vdash -1$ $\vdash -16$ $\equiv -3$	
$\vdash 37 \vdash 9 \vdash 2$ $\vdash 70 \vdash 3 \vdash \vdash$ $\vdash 24 \vdash 12$ $\vdash 20 \vdash 13$ $\vdash 35 \vdash 12n2 \vdash 2$ $\vdash 100 \vdash 12 \vdash$ $\vdash 120 \vdash 12n2 \vdash$	$\equiv -3$ $\vdash -60 \vdash$ $\vdash -5$ $48 \neq -1$ $\vdash \neq -3$ $\vdash -12 \vdash$ $\vdash -1$	
$\vdash 65 \vdash 11 \vdash 3$ $\vdash 65 \vdash 25n13 \vdash 3$	$\vdash n \vdash$ $\vdash \leq \vdash -4$	$\leq$ $110n13 \vdash 110n13$
$\vdash 80 \vdash 18 \vdash 4 \vdash$ $\vdash 90 \vdash 10 \vdash 5 \vdash 2$ $\vdash 105 \vdash 6 \vdash 5 \vdash 3 \vdash 3$ $\vdash 10 \vdash 15 \vdash 7 \vdash 5 \vdash 3 \vdash$ $\vdash 10 \vdash 18 \vdash 11 \vdash 10 \vdash 3 \vdash$	$\vdash \leq -1 \vdash$ $\vdash \leq -2 \vdash$ ≤ -1 $\equiv -4$ $\equiv -5$	
$\vdash 95 \vdash 7n5 \vdash$ $\vdash 30 \vdash 5 \vdash 2n2 \vdash$	$12 \vdash \vdash / \vdash \leq \vdash$ $\vdash \equiv \vdash$	
$\vdash 80 \vdash 4 \vdash$ $\vdash 320 \vdash 23 \vdash 2n \vdash$ $\vdash 320 \vdash 25 \vdash 2n \vdash$ $\vdash 350 \vdash 26n2 \vdash \vdash$	$13 \vdash \vdash / \vdash \leq \vdash$ $\vdash 620$ $\vdash 590$ $\vdash -5$	

$\mathbb{F}300$ 28 4 γ 4 $\mathbb{F}225$ 10 $\cap$ 10 γ $\mathbb{F}110$ 14 $\sqcup$ 13 2 $\mathbb{F}175\propto$ 8 6 γ $\sqcup$	$\top$ -1 $\top$ -11 $\sqcup$ -6 $\top$ -16	
$\mathbb{F}08$ 17 8 γ 6 $\cap$ $\mathbb{F}09$ 16 9 γ 5 $\cap$ 2 2 $\sqcup$ $\mathbb{F}09$ 31 8 $\vee$ 2 $\mathbb{F}13$ 16 8 5 γ 5 $\cap$ 4 ∞ $\mathbb{F}15$ 15 10 γ 5 3 $\cap$ $\mathbb{F}15$ 28 10 γ 3 $\cap$ $\mathbb{F}15$ 28 10 γ 3 2 $\cap$ $\sqcup$ $\mathbb{F}200$ 29 6 $\cap$ 2 $\mathbb{F}190\Delta$ 62 29 $\sqcup$ 5 γ 2	$\top$ -6 , $\top$ -6 $\cap$ $\sqcup$ $\leq$ -1 $\sqcup$ - $\leq$ -13 / 1- $\infty\Delta$ $\top$ -12 , $\top$ -12 $\cap$ $\top$ -18 $\top$ -19 $\top$ -20 $\top$ -3 $\top$ -2	

$\top$ -2 | ,
 $\top$ ∞ 6-2, ∞ | Δ ∞ $\top$ $\cap$ $\sqcup$ 11546-75.
 $(\gamma$ -2 |) -

 $\top$:

24 Δ 26%, 6 Δ 8,5%, 7 Δ 10%,

3%, 0,4%, 0,3%,

 54 HRC.
 ∞ (∞) 50 %

50%

 63 HRC.
 Δ (Δ ∞) 5%

 5% 30% 60%

60 HRC.

12600 1300°

().

250 31% 30 5% 2,50 3%

2,80 3,5% 1,5%

21448-75

27, 1, 25,

6-2, 1, 2, 3, 4

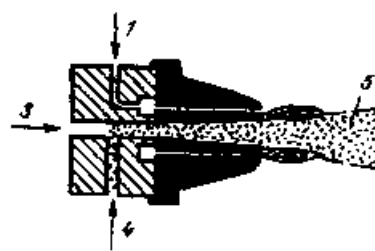
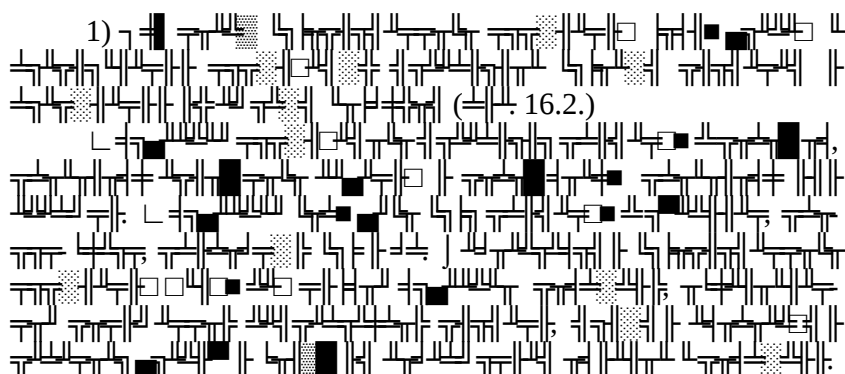
21449-75,

27, 1, 2, 30 30-

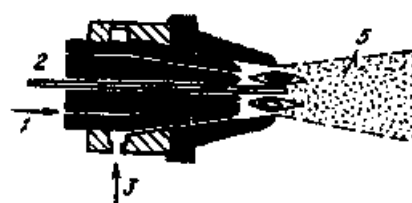
300 350, 5 6 350 400; 8

450 500.

- △
1. ?
 2. f ?
 3. △ ?
 4. ?
 5. △ ?

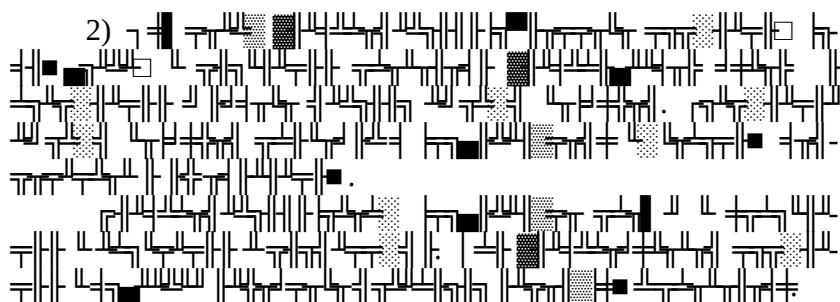


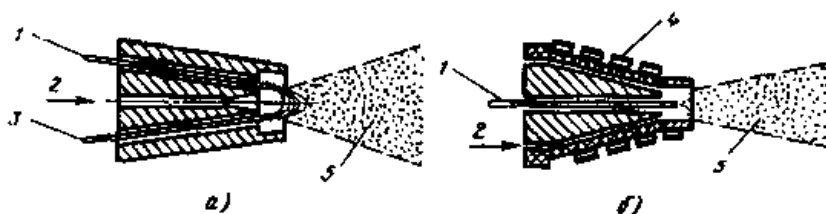
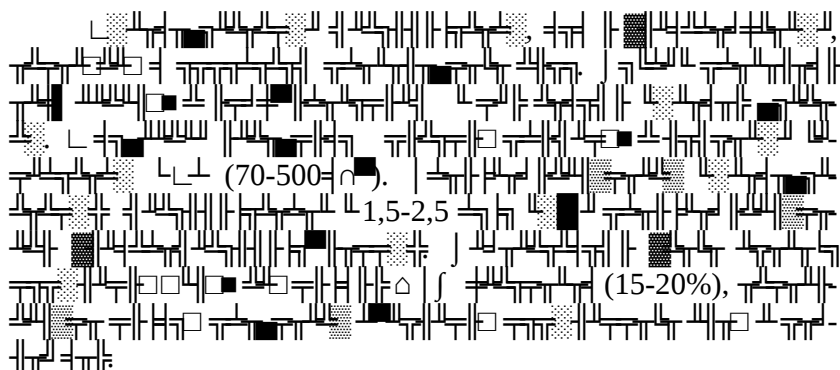
a)



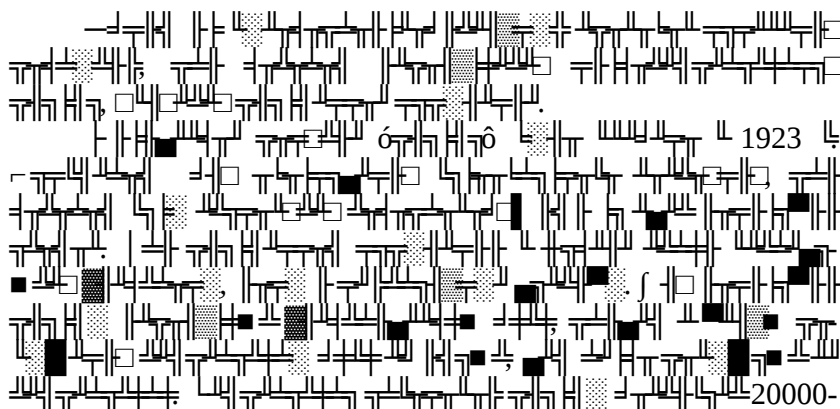
б)

Fig. 17.2. 1 -  2 -  3 -  4 -  5 - .

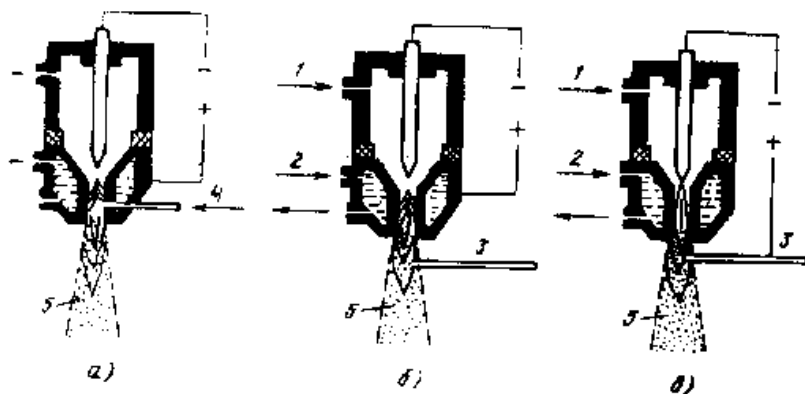




16.2.



23000 ° 7.

$$= 0,03$$


16.4.

Figure 1 is a schematic diagram of the experimental setup. It shows a participant sitting at a table, viewing a screen. The screen displays a sequence of stimuli: a fixation cross, a target stimulus (a black square), and a distractor stimulus (a white square). The participant's response is recorded via a button press.

1) 5-100, 160, 70-200⁰ (

2) 2-3, 100-200⁰.

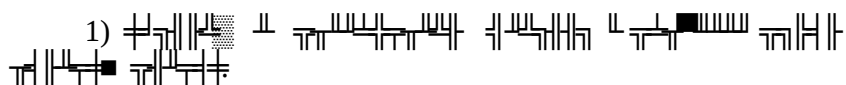
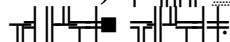
3) (✓),

-
1. ?
 2. ?
 3. ?
 4. ?
 5. ?
 6. ?

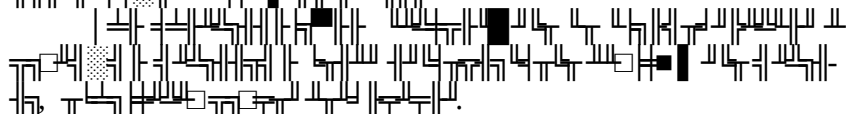
17.

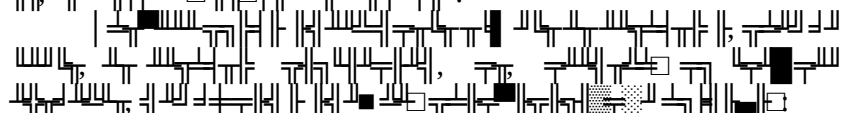
-
- 17.1. ?
 - 17.2. ?

17.1.

1)  

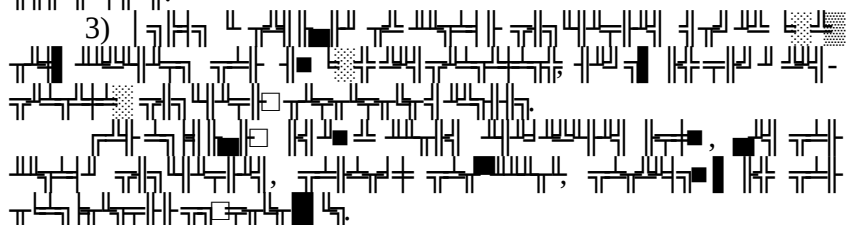
2) 





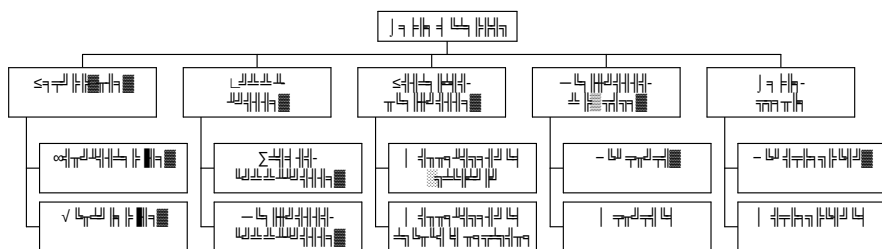
1) 

2) 

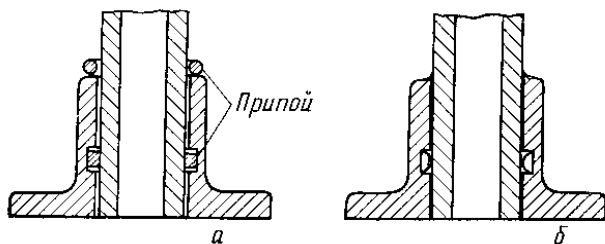
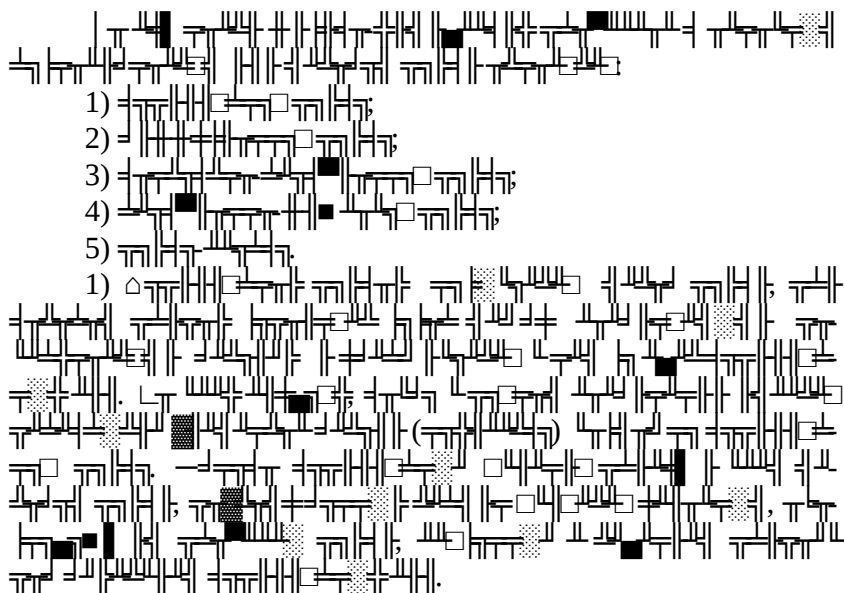
3) 

17.2.





ר. 17.1. חלקי המבנה



ר. 17.2. חלקי המבנה

2) f

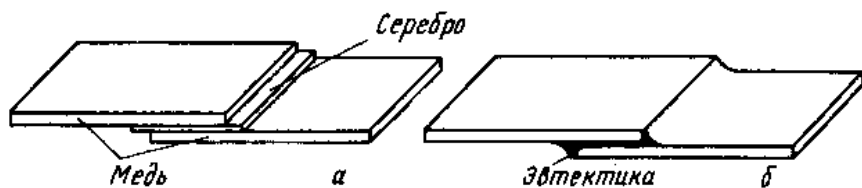
W Pt-B

855č

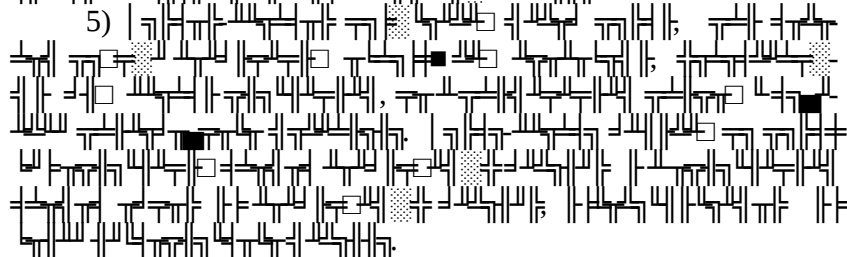
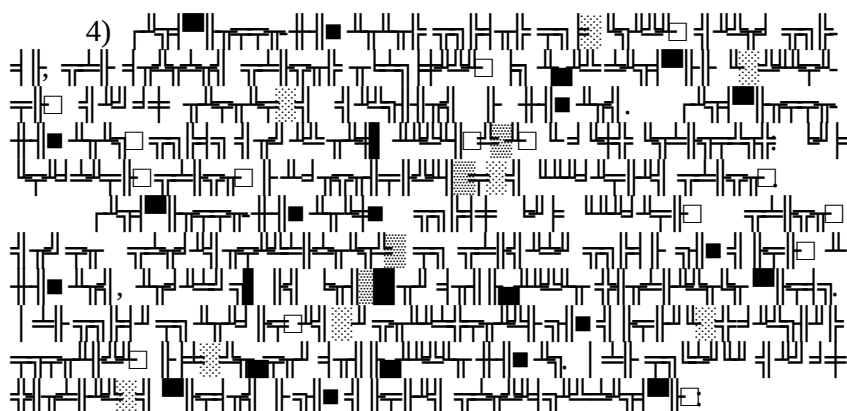
$$3W + Pt B \rightarrow PtW + W_2B$$

2000č.

3) Δ

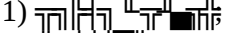
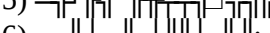
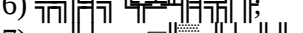


17.3.

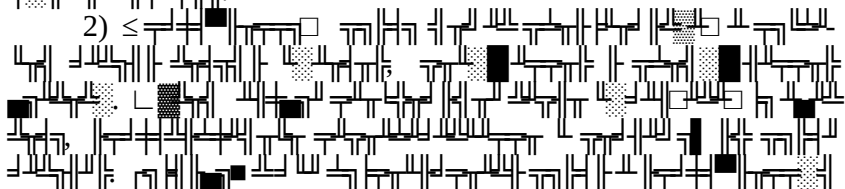
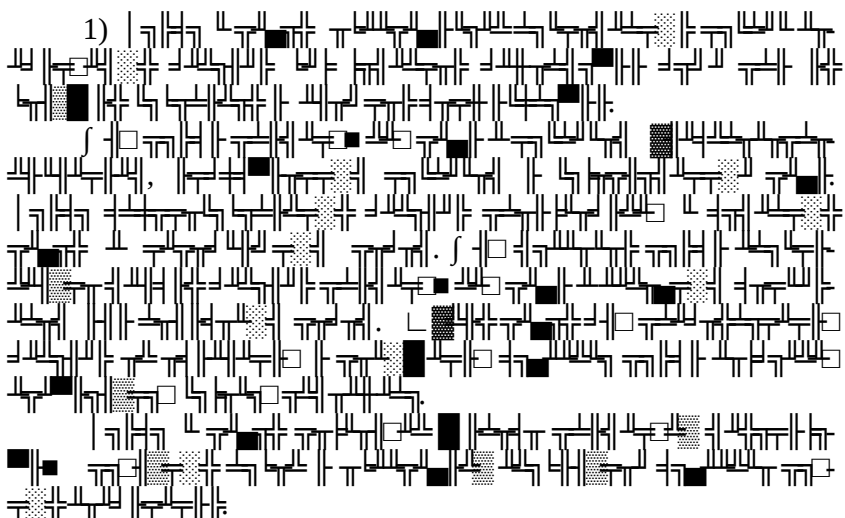


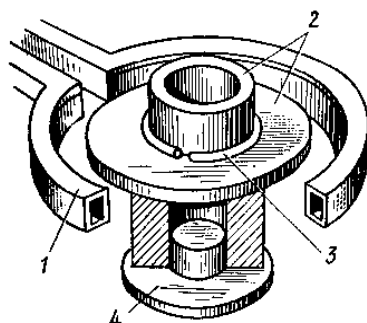
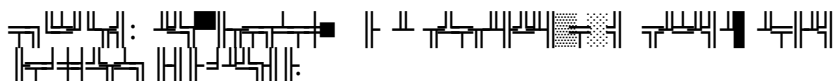
18.1. $\triangle$



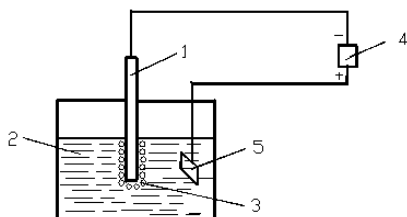
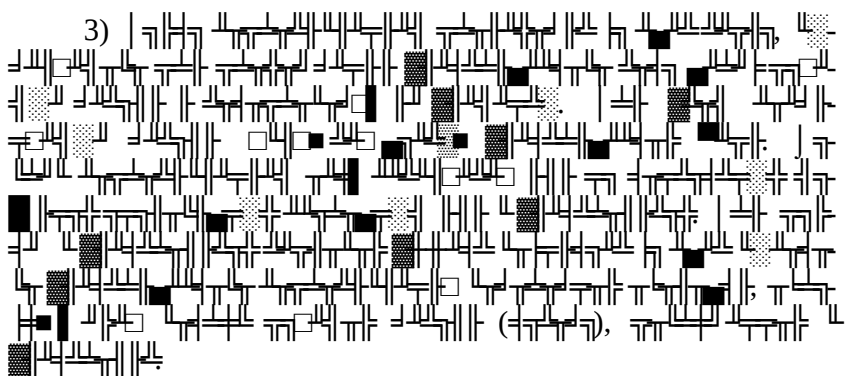
- 1) 
- 2) 
- 3) 
- 4) 
- 5) 
- 6) 
- 7) 

18.2. γ





18.1. 1 - 2 - 3 - 4



18.2. 1 - 2 - 3 - 4 - 5

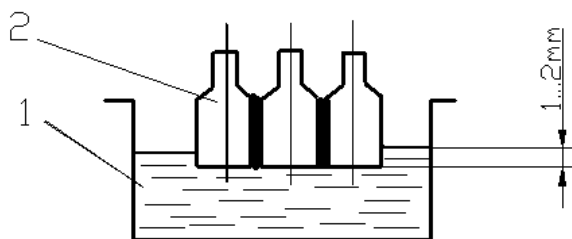
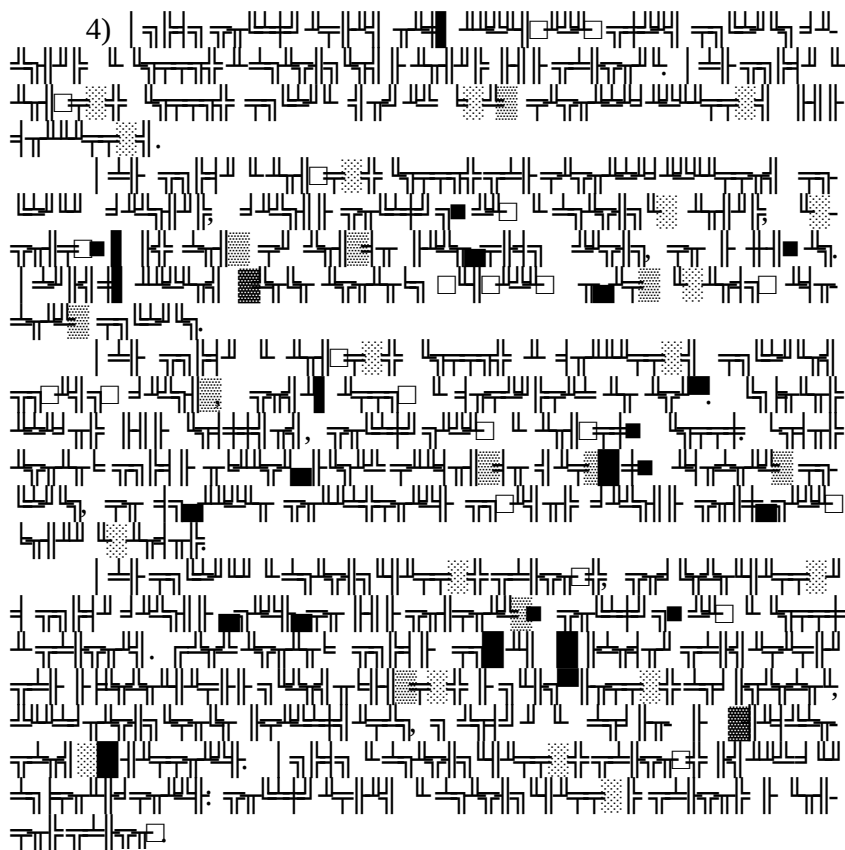
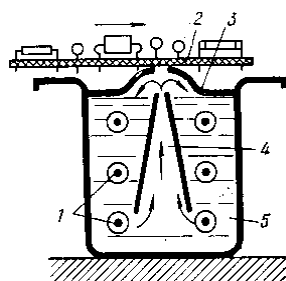
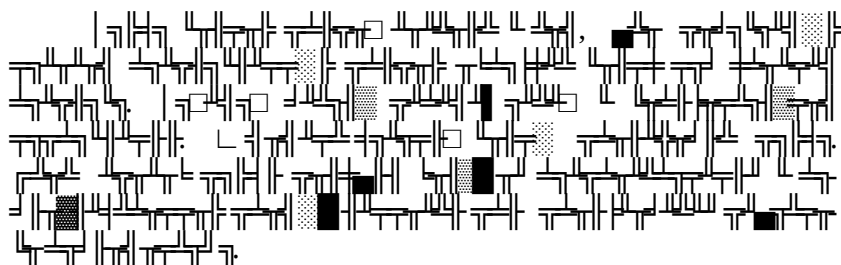
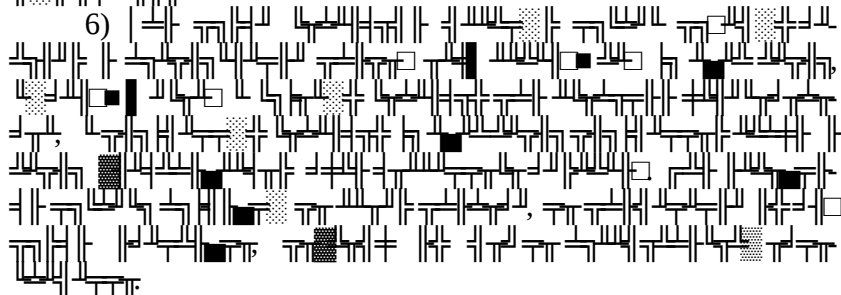
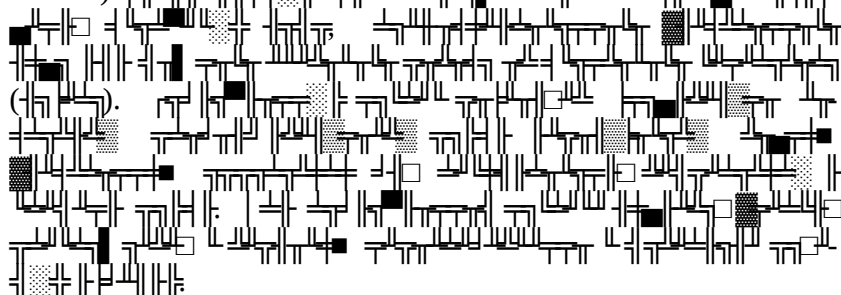


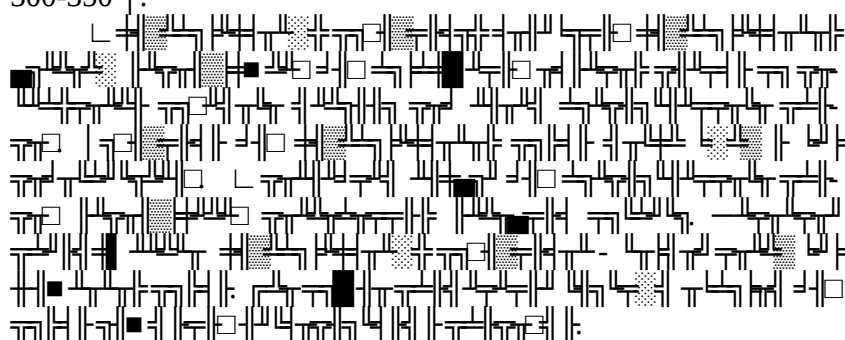
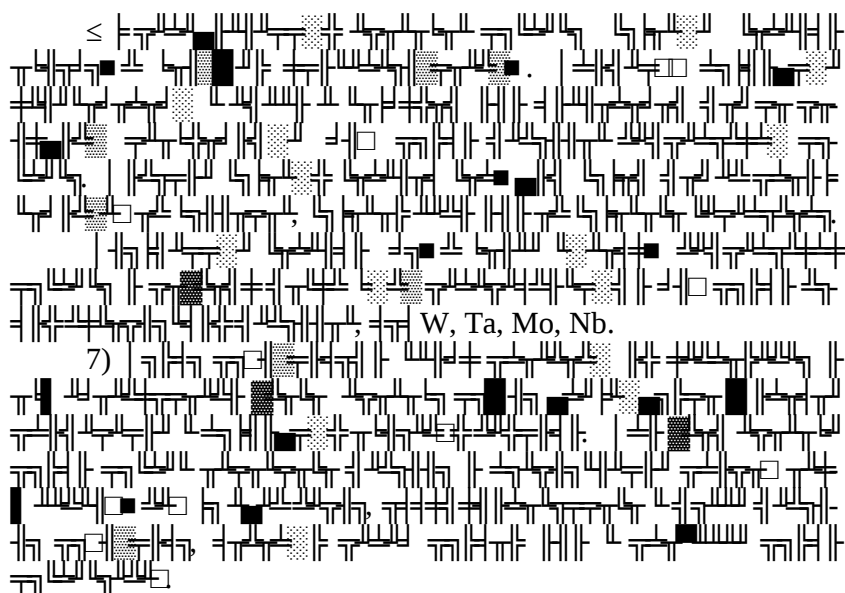
Рис. 19.4. 1 - ... 2 - ...



19.5.

1 - ; 2 - ; 3 - ; 4 - ; 5 -



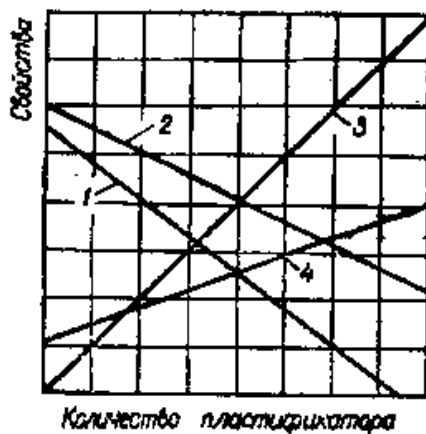
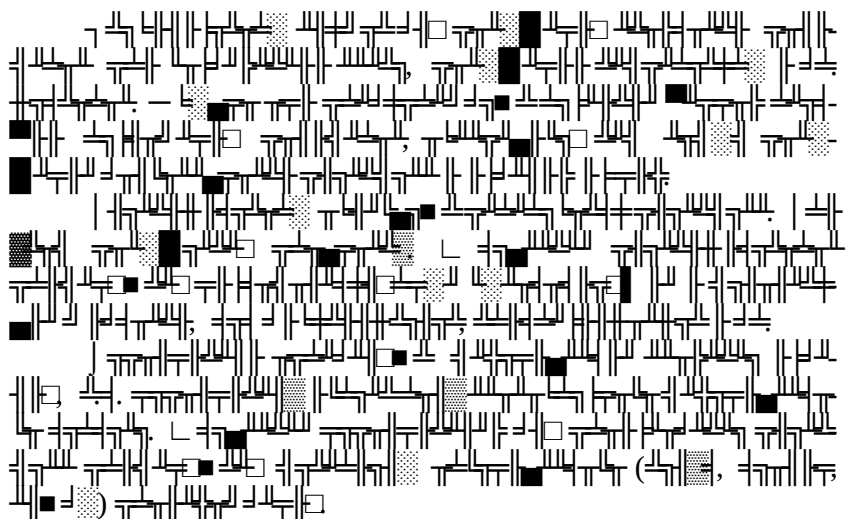


1. ?
2. ?
3. ?
4. ?
5. ?

19.

- 19.1. ?
- 19.2. ?
- 19.3. ?

19.1.

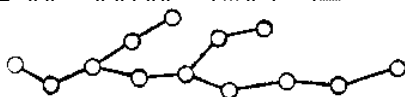
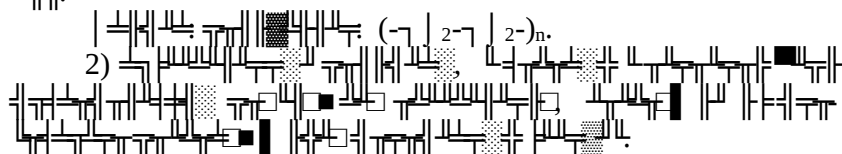
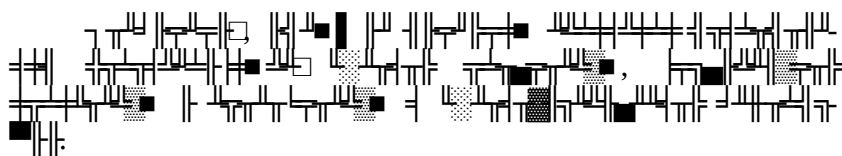


19.1. $\leq$

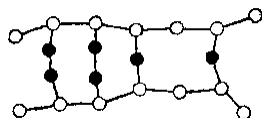
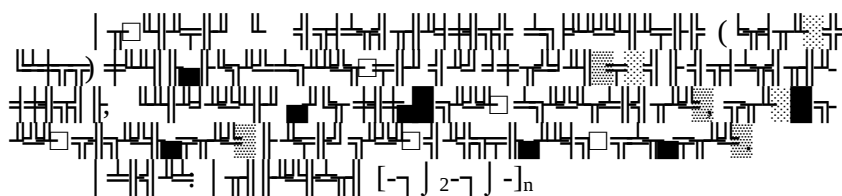
1 - 2 - 3 - 4 -

$\frac{1}{n} \sum_{i=1}^n \left(\frac{\partial L(\theta)}{\partial \theta_i} \right)^2 = \frac{1}{n} \sum_{i=1}^n \left(\frac{\partial L(\theta)}{\partial \theta_i} \right)^2$

19.2. $\neg$

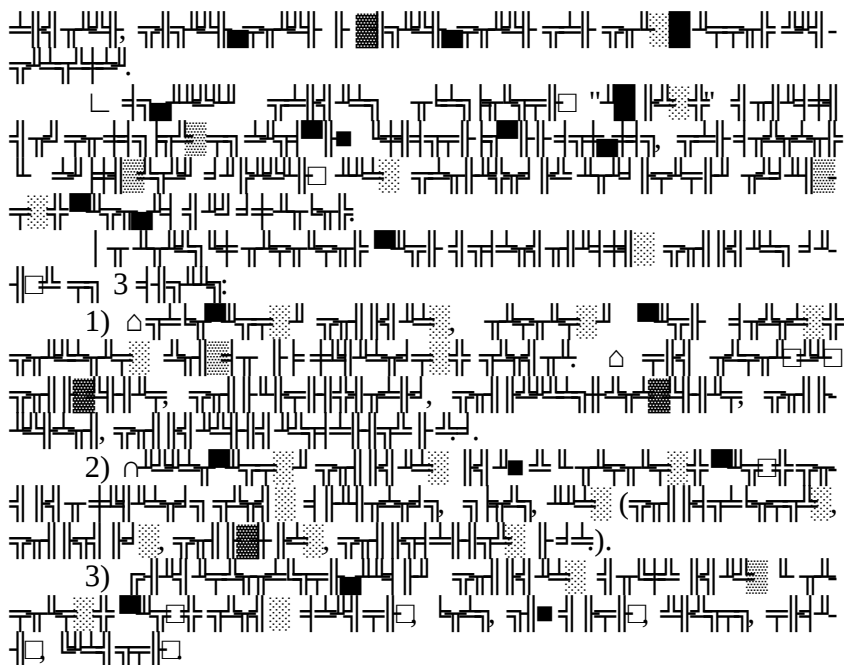


19.3.

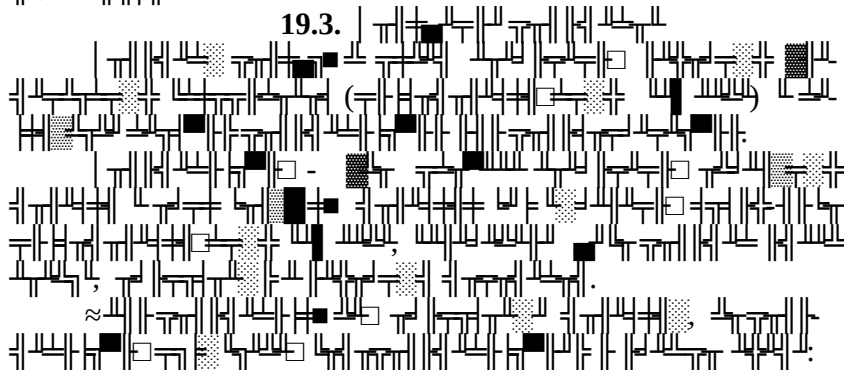


19.4.





19.3.



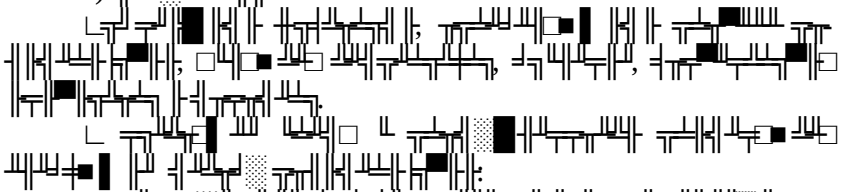
$$nA \rightarrow (-A)_n,$$



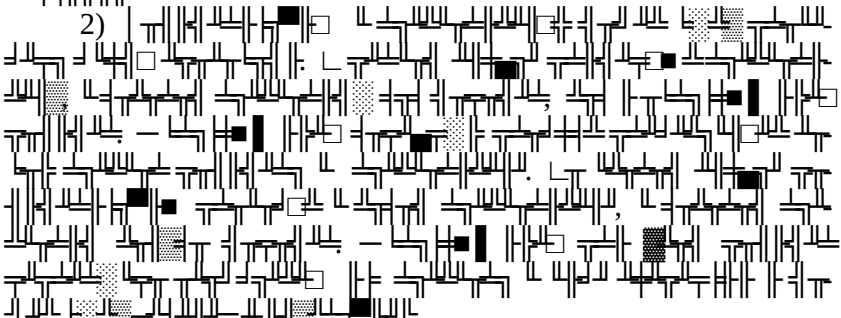
$$nA + nB \rightarrow (-A-B)_n.$$



- 1)
- 2)
- 3)



- 1) ∞
- 2)
- 3)



- 1)
- 2)
- 3)

20. 7

- 20.1. 7
20.2. 7
20.3. 7
20.4. 7
20.5. 7

7

20.1. 7

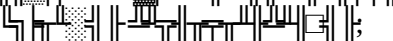
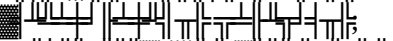
2

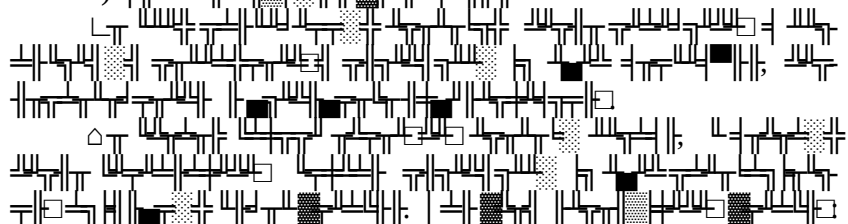
1)

7

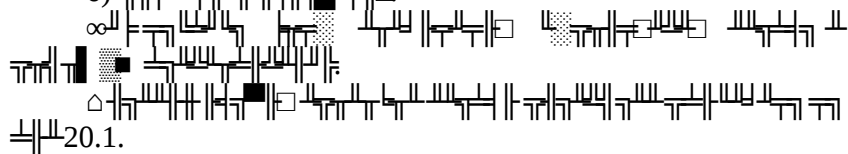
20.3.

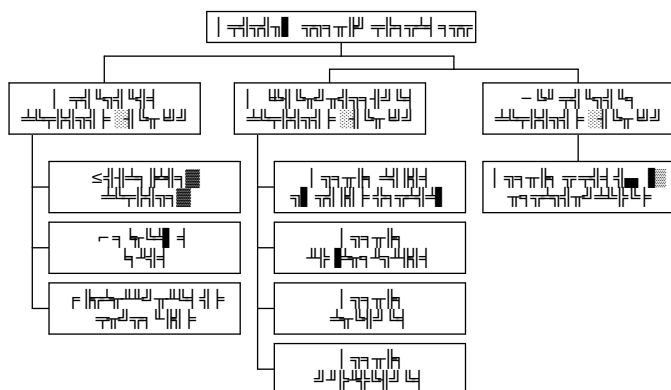


- 1) 
- 2) 
- 3) 

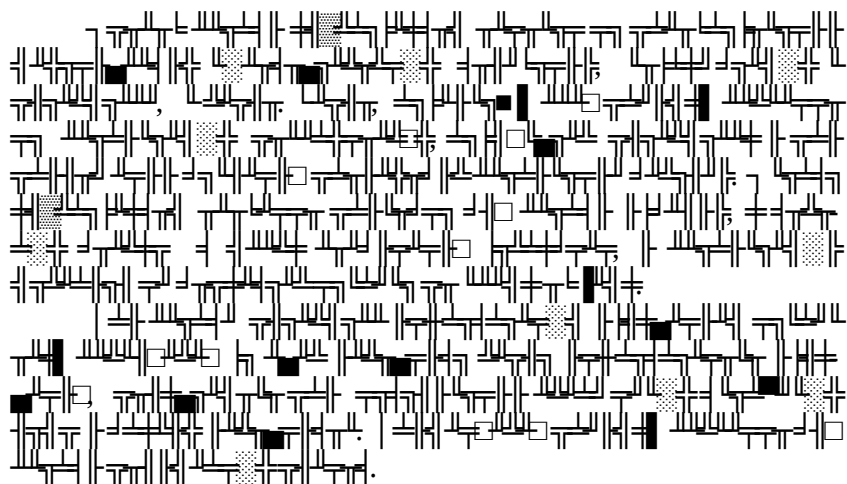


- 1) 
- 2) 
- 3) 
- 4) 
- 5) 
- 6) 

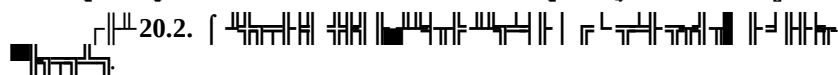
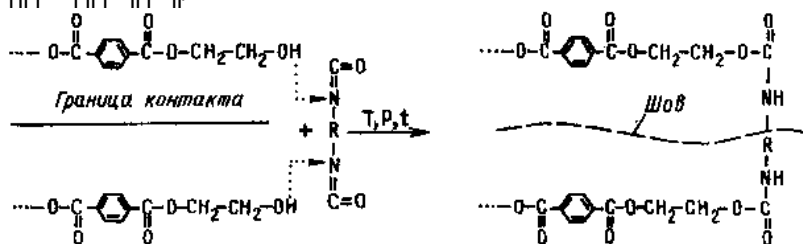
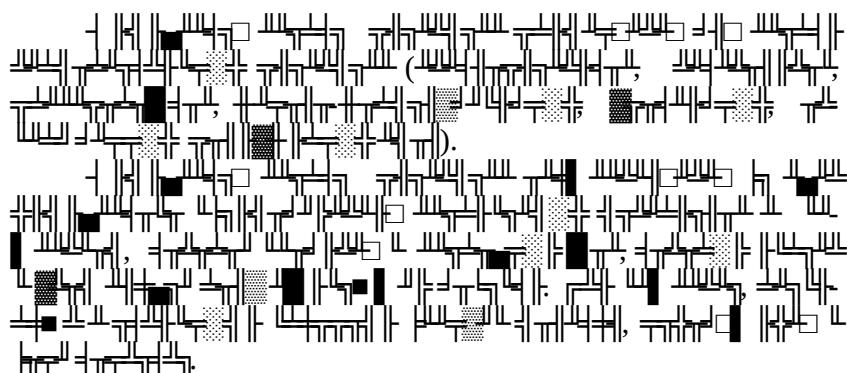


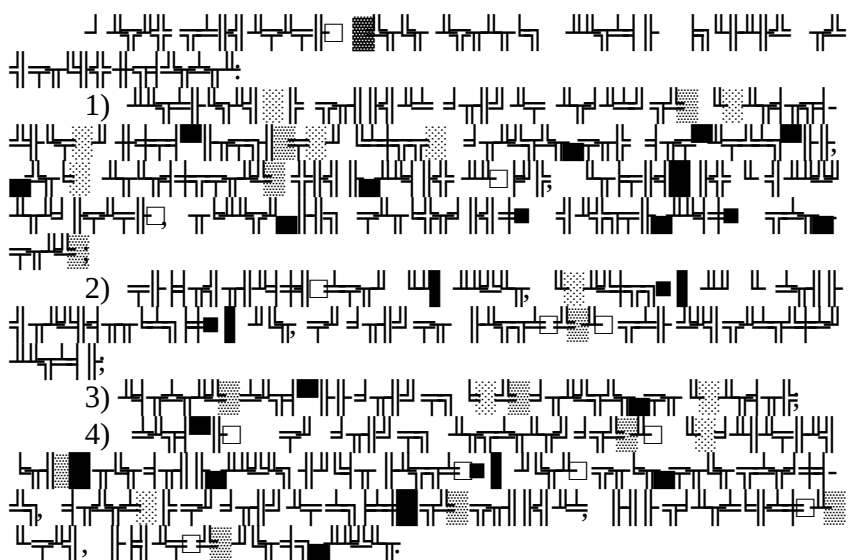


20.1. Δ

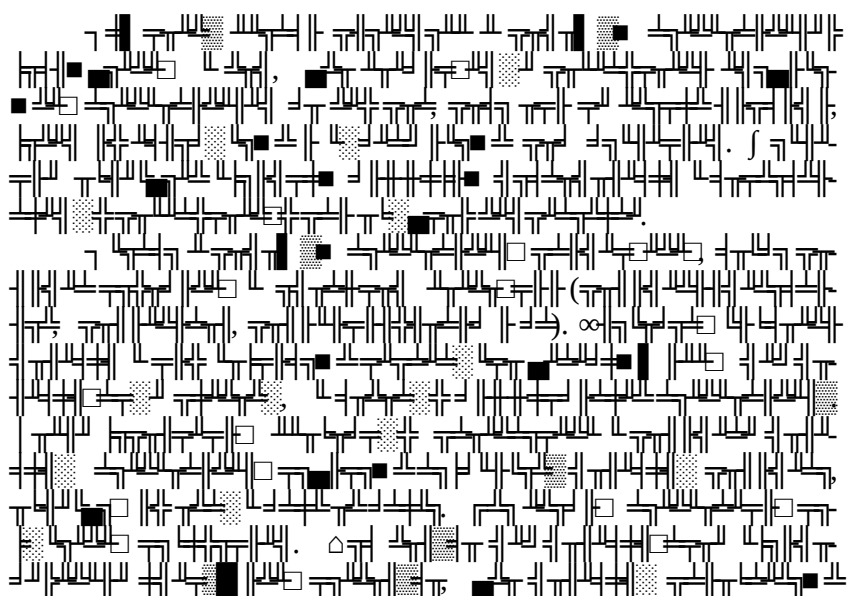


20.4.





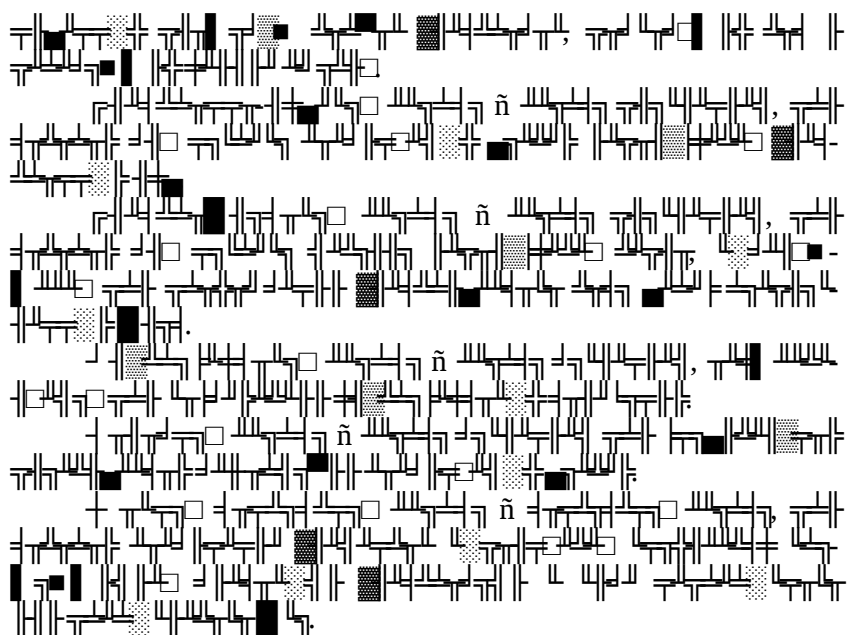
20.5. γ





1. 2. 3. 4. 5.

[illegible]



$$r \leq \frac{L}{\sqrt{r}} \sqrt{\frac{L}{r}}$$

1. Edward R. Bohard. Welding: Principles and Practces - American Welding Society - Connect Learn Success, 2012

2. Messler R. Principles of welding. - London: Wiley ñ Inter-science, 2005.

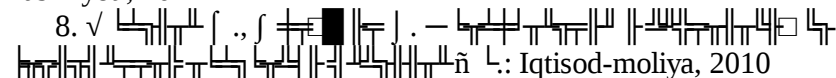
3.  2014

4. Abralov M.A., Dunyashin N.S., Abralov M.M., Ermatov Z.D. Eritib payvandlash texnologiyasi va jihozlari ñ T.: Voris, 2007

5. Abralov M.A., Dunyashin N.S., Ermatov Z.D. Gaz alangasi yordamida metellarga ishlov berish texnologiyasi va jihozlari ñ T.: Ilm ziyo, 2007

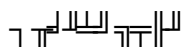
6. Abralov M.A., Dunyashin N.S. Kontaktli payvandlash texnologiyasi va jihozlari ñ T.: Turon-iqbol, 2006

7. Abralov M.A., Ermatov Z.D., Dunyashin N.S. Qo'lda yoyli payvandlash jihozlari ñ T.: O'zbekiston faylsuflari milliy jamiyati nashriyoti, 2012

8.  ñ T.: Iqtisod-moliya, 2010

9.  2004

10. www.welding.com

[illegible]